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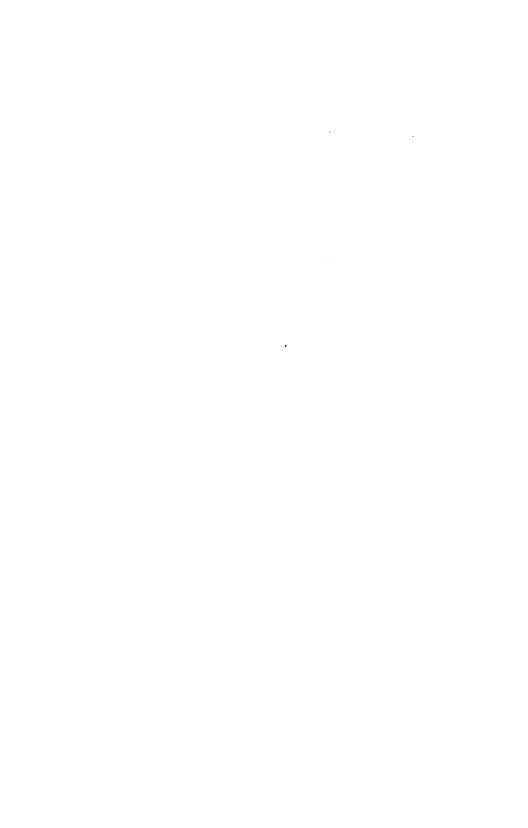
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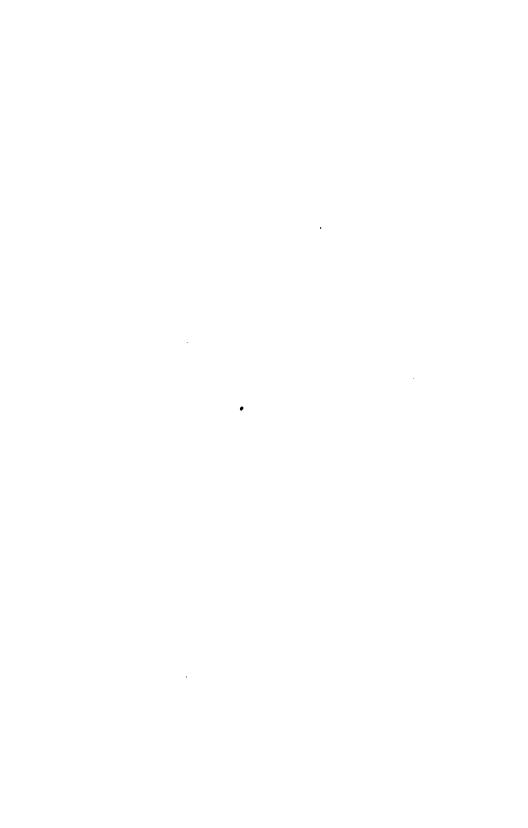
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EXCAVATION AND EMBANKMENT

# TABLES;

APPLICABLE

## TO ALL WIDTHS OF ROAD BED,

#### AND ALL SLOPES:

CALCULATED FOR ALL DEPTHS LESS THAN 60 FEET.

BY WM. H. MORRISON,

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### INTRODUCTORY REMARKS.

The following is a brief outline of the manner in which quantities are calculated by these tables.

The cross average of the side and center depths is first taken.

A method is pointed out of determining what amount of error is caused by taking the cross average as the end depth in any given case. Rules are also given for the correction of the cross average, if this is necessary. Thus the end depths may be obtained with any degree of accuracy that may be desired. In whatever way they are found, the tables for finding the solid contents are equally applicable. The solid contents may be obtained in two ways.

In calculating by the first method, the vertical distance at which the planes of the slopes produced, intersect each other above the roadway in embankment, or below it in excavation, is added to the actual depths.

The contents for these total depths are then taken from the tables for a slope of 2½ to 1. At the end of each section, this slope of 2½ to 1 is reduced to the actual slope by the use of the proper multiplier: and afterwards the solid contents of that portion lying above the roadway in embankment, or below it in excavation, which is contained between the roadway and the planes of the slopes produced are deducted at once for the whole length of the excavation or embankment in the section, which gives the actual number of cubic yards contained in the section.

In calculating by the second method, the quantities contained in the central part of the excavation or embankment, are kept separate throughout each section from those con-

tained in the slopes. The former are first found for a width of 10 feet; the latter for a slope of 2½ to 1. The sums at the end of each section are then multiplied by the proper multipliers, which gives the actual amount of excavation and embankment in the section.

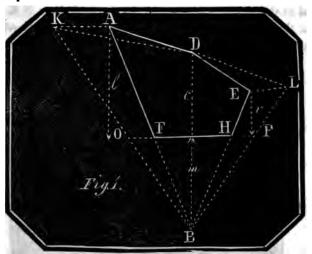
From the supplements to the tables for finding the solid contents, the quantities for any length less than 100 feet may be taken directly, whenever the depth of the mass is less than 20 feet, (if the calculation is made by the second method; and whenever the depth of the mass is less than 30 feet, if made by the first method) without multiplying or dividing in order to obtain these quantities from the contents of stations 100 feet long; and the corrections for the differences of the end depths are obtained in a similar manner whenever the difference of ends does not exceed 15 feet.

WM. HENRY MORRISON.

Indianapolis, March 26, 1853.

## EXPLANATIONS.

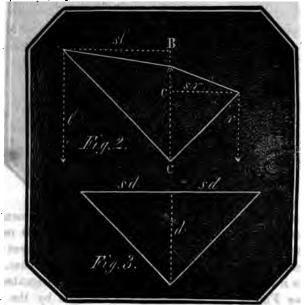
First. Of the method of finding the depths of end areas which are equal to the given end areas, and level at the top.



If the lines of slope in excavation or embankment be produced as shown in Fig. 1, (in which AFHED represents the end area of an excavation) they will meet at a certain distance below the roadway in the former case, and above it in the latter. Let this distance be designated by m (see Fig. 1). In calculating the contents by the first method given, m is added to the actual depths.

The depths thus increased may be designated as the total depths.

We wish first to show that in any two given cases, where different slopes are used, if the total depths at the sides and center are respectively equal, the total depths of the equivalent end areas, level at the top, will also be equal. Thus in Fig. 1, A F H E D and K O P L D representing the end areas of excavations which have different slopes; these slopes intersecting at B; and the total depths of cutting at the sides and center (measured from a horizontal line passing through B) being respectively equal; then if the area A B E D be reduced to an equivalent area, level at the top, lying between the lines of slope B A and B E, and the area K B L D be in like manner reduced to an equivalent area, level at the top, lying between the lines of slope B K and B L, the total depths of the areas, which are level at the top, will be equal.



In Fig. 2, let

l=the total depth at the left side,

c= " " " centre,

r=" " " right side,

ama number which, multiplied by any total depth will give

the horizontal distance out, of the slope, at that depth measured from the vertical line B C\*, we shall have (Fig. 2) the

end area = 
$$\frac{s r c}{2} + \frac{s l c}{2} = \frac{s c (r+l)}{2}$$
 (Eq. 1.)

Again, let Fig. 3 represent an equivalent end area, level at the top, whose *total* depth we will designate by d, s having the same value as before. We shall have the end area  $= s d^2$ . (Eq. 2.)

Substituting this value for the end area in Equation 1, we have

$$s d^2 = \frac{s c (r+l)}{2}$$
 hence  $d^2 = \frac{c (r+l)}{2}$ 

From this equation it is evident that the *total* depth of the equivalent end area, level at the top, depends solely for its value on the *total* depths at the sides and center, and not on the slope; and, therefore, if we find this total depth for one slope, for any given total depths at the sides and center, it will answer for any slope whatever.

By the following tables, the *total* end depths, whenever it is necessary to change the cross average, are found for a slope of 2 base to 1 perpendicular. They are obtained by correcting the cross average, or by another method which will be hereafter noticed.

OF THE CORRECTION OF THE CROSS AVERAGE, WHEN THIS DOES

NOT GIVE THE TRUE DEPTH.

We must first determine the amount of error occasioned by taking the cross average as the true end depth.

Having taken the differences separately between the center depth and each side depth, let the greater of these

* The value of s is always indicated by the slope, thus														
For a	alope of	11	base	to one	perpendicular,	-	•	-	-	•	•	•	•	s = 1.25
	"													s=1.5
44	44	1#		**	**		-	-		-		•	÷	s=1.75
44	44	0					_	•		_	_	_	_	9

<sup>†</sup> The cross average is found by dividing the sum of the side depths plus twice the centre depth, by 4.

two differences be represented by E, and the lesser difference by D.

If, now, we average the center with each side depth separately, it will be found, by drawing the figure, that the amount of area gained by thus averaging will be

$$=\frac{s(E^2+D^2)}{8}$$
 (Eq. 3.)

If, again, we average the two depths thus obtained, it will be found, by drawing the figures, that when both side depths are greater, or both less than the center depth, the amount of area lost will be  $=\frac{s(E-D)^2}{16}$ .

Hence, the total gain in these cases will be

$$=\frac{s(E^2+D^2)}{8}-\frac{s(E-D)^2}{16}=\frac{s(E+D)^2}{16}$$
 (Eq. 4.)

It will also be found that in all other cases the amount of area lost by the second average will be  $=\frac{s(E+D)^2}{16}$ .

Hence, the total gain in these cases will be

$$\frac{s(E^2+D^2)}{8} - \frac{s(E+D)^2}{16} = \frac{s(E-D)^2}{16} \quad (Eq. 5.)$$

(For the further demonstration of this, see page 18.)

If we represent by v the quantity E+D in Eq. 4, and E-D in Eq. 5, we shall have, total gain of area by cross averaging,  $=\frac{s}{16}$  (Eq. 6.) And in order to find the value of v, we have the following rule:

RULE I. Take the differences separately between the center and each side depth. Then, if both of the side depths are greater, or both less than the center depth, add these differences together (see Eq. 4.); in all other cases subtract one from the other (see Eq. 5.); the result is the value of v.

As before stated, the slope for which the total end depths are found by these tables, whenever the cross average is not sufficiently accurate, is that of 2 base to 1 perpendicular.

The value of s for this slope being 2, we have from Eq. 6—gain of area by cross averaging  $=\frac{v^2}{8}$ .

In order to find readily the end depths, two tables have been formed; Table 1 which contains the end areas in square feet, for a slope of 2 to 1, for each half tenth of a foot in depth, commencing with a depth of .025; and Table 2 which contains the values of  $\frac{v^2}{8}$  for each value of v from

.1 up to 32 feet. Table 1 is carried to a depth of 71.9 feet. To find the *total* depth of the equivalent end area, level at the top, when the cross average requires to be changed, we have the following rule:

RULE II. To the cross average add the value of  $m^*$  (see Fig. 1.). Find the depth in Table 1, which is nearest to their sum, and take from the table one of the areas next to that depth. Having obtained by Rule I. the value of v, subtract from the area taken from Table 1, the number found opposite the value of v in Table 2, and apply the remainder again to Table 1; observe between what areas in this table the remainder falls; opposite will be found the total depth of the end area, which is equivalent to the given end area, and level at the top.

When the value of v exceeds 32 feet, or when great accuracy is desired, the following method of finding the total end depths may be adopted. (See Eq. 1, from which, since in this case s=2, we shall have the end area =c(r+l).)

SECOND METHOD. Multiply the sum of the side depths plus twice m, by the center depth plus m, and apply the product to Table 1. Observe between what areas this product falls; opposite will be found, as before, the total depth of the equivalent end area, level at the top.

The exact area may also be obtained from Table 1 by

<sup>\*</sup> The value of m is found by dividing helf the width of the road bed by the value of s. Thus if the width of the road bed is 20 feet and the slope 14 to 1, then  $m = \frac{10}{1.25} = 8$ .

using, together with the area taken from the column of areas, a proportionate part of the tabular difference taken from the column headed D.

It will be remembered that the TOTAL end depths thus found are equally correct for all slopes and all widths of road bed, if we use in each case the proper value of m.

une	cross	average	pius.		15			
46	-	**		66	• • • • • • • • • • • • • • • • • • • •	4.0 v=	=	1.9
66					***************************************			
46	"	40			•••••			
æ	"		".	"	• •••••••	10.0 v=	=	2.9
*	66	<b>66</b>	**	60	•	15.0 v:	=	3.5
"	166	"	84	L	d	20.0 v	=	4.1
u	44	00	CL		ddd			
**	4	te	**	L	• • • • • • • • • • • • • • • • • • • •	30.0 v:	=	5.0
••	46	LE	LE	66		40.0 v	=	5.7
"	"	EL	"	6		50.0 v =	=	6.4

### MODE OF OBTAINING THE SOLID CONTENTS.

FIRST METHOD. In calculating by the first method, we use the total depths in all cases.

When they have not been found by Rule 2, add the value of m to the cross average in order to obtain them.

The total end depths of each mass are then added together and divided by 2.\* The contents for this average total depth are then taken, both in excavation and embankment, from Table 4 or its supplement, which are calculated for a slope of 2½ base to 1 perpendicular. In addition to the quantities thus obtained, a correction is required which varies according to the difference of the end depths, and

<sup>\*</sup> Where a transition is made from cut to fill, the total depth must be reckoned for excavation in one direction, and for embankment in the other.

the length of the mass; (this correction in cubic yards is  $=\frac{s l d^2}{324}$  in which s= slope, d= difference of end depths, l= length: all of these dimensions being in feet.) This correction is, in all cases to be added to the former amount, as the contents for the average of the end depths are less than the true amounts.

These corrections for a slope of 2s to 1 are given in Table 5 and its supplement.

Having thus found the contents for a slope of 2s to 1, this slope is reduced at the end of each section to the actual slope by using the proper multiplier. This multiplier is equal to s divided by 2.5, or equal to one-tenth of the number of quarters contained in s. For a slope of

S	ıltiplier	he mu	pendicular	1 perp	e to	bas	1
**************	46	44		1		**	1‡
**************************************	"	46	"	1	,	"	11
,,,	66	66	46	1	•	"	17
************	"		"	1			2

Having thus reduced the slope of 2t to 1 to the actual slope, we must next remove the prism lying between the plane of the roadway and the planes of the slopes produced, for the whole length of excavation or embankment, as the case may be, in the section. If we designate this length in feet by L, the contents of the prism will be, in cubic yards,  $\frac{s}{2} \frac{m^2}{2} \frac{L}{2}$ 

To find the contents for the *tetal* depths for a slope of 2t to 1, and *for lengths of* 100 *feet*, and to reduce this to the actual slopes, we have the following rule:

RULE III. Take from Table 4 the amount opposite the average of the total end depths, and also from Table 5 the amount opposite the difference of the end depths, placing the amounts for excavation and embankment in separate columns; and at the end of the section multiply their sums

<sup>\*</sup> See Gillespis on Roads and Railroads, page 327.

by the proper multipliers as before directed, in order to reduce the slope of 24 to 1 to the slopes actually used.

If the length of the mass is less than 100 feet, a portion of the amounts contained in Tables 4 or 5, proportional to its length must be taken, instead of the full amounts.

For all depths less than 30 feet, and for all differences of ends less than 15 feet, the trouble of multiplying or dividing, in order to effect this, is saved by the supplements to Tables 4 and 5.

In these supplements the contents for lengths of 10 feet, 20 feet, 30 feet, &c., up to a length of 100 feet are given.

The contents for any length less than 10 feet are also easily obtained by mentally removing the decimal points one figure to the left. Thus, in the supplement to Table 4, for a depth of 7.2 feet, the contents for a length of 50 feet are 240 cubic yards, and by removing the decimal point one figure to the left, we find the contents for a length of 5 feet are 24 cubic yards.

When two quantities are taken from the same table, for a length less than 100 feet, it will be less trouble to write them separately in their proper column than to add them together when taken from the table: thus, if we wish to find the contents from the supplement to Table 4, for a depth of 11.5 and for a length of 84 feet;

The contents for a length of 80 feet are.....979.60 cubic

" " 4 " ..... 48.98 vds.

It will be found best to place the corrections taken from Table 5, or its supplement, in a separate column, instead of adding them to the contents for the average of the end depths.

RULE IV. Having obtained the quantities for a slope of 24 to 1, and reduced this to the actual slope, as directed in Rule III.; deduct the prism lying between the roadway and the planes of the slopes produced, for the total length of the excavation or embankment in the section. (The contents of this prism, in cubic yards, are equal to the product

of  $m^2$  by the value of s; multiplied by the length of excavation or embankment, as the case may be, in the section, divided by 27.) The remainder will be the actual number of cubic yards of excavation or embankment in the section.

Examples of this method of calculating are given on page 14. In these examples, when the length of the mass was considerable, the surface of the excavation, and the base of the embankment on each side of the centre line of the road, were made as slightly warped as possible; for no practicable method of calculation will give a true result if the surface of the ground is much warped. The remedy in such a case is to set additional intermediate stakes, so as to reduce the error to an inconsiderable amount. In the examples here given, the slope in excavation is 14 to 1, and the width of road bed 20 feet; in embankment the slope is 11 to 1, and the width of road bed 14 feet. The depths in excavation have the sign plus, those in embankment the sign minus prefixed to them. The value of m in excavation is 8: in embankment 4.67.

In calculating by this method, the lengths of the masses of excavation and embankment should be placed in separate columns, so that they can be easily added up at the end of the section.

For convenience in changing the cross average, (when that is sufficiently accurate,) to its corresponding total depth, it will be best to form a table in which are written in one column the actual depths, and opposite to them the sums of these actual depths plus m.

In all the tables for finding the solid contents, the quantities are given in cubic yards; and except in the supplements the length of the stations is taken at 100 feet.

H	•anoit			1.2 1826.8	1828.0			
EMBANKMENT.	of 24 to 1 Correc-				<del>! `</del>	4.0	.9	7249.5
ENTER	Sont'nto eqois rot			26.0 10400.0	10426.0 1828.0	12254.0	7352.40 102.9	
TION.	Correc-	2351.1	~~		2354.1		Deduct a- mount ab. road bed,	Cubic yde. embank't, By prism'i formula.
EXCAVATION.	Sont'nts eqols tol for \$2 to	= -	102.1	,	15491.0 2354.1	17845.1 .5	8922.55	8581.8 8580.4
-A	7	+40.7	+10.55				Deduct amount below road bed,	Cubic yards excavation,
	Diff. of E	55.2	5.1	5.6			road	-
P	Total En Depths	9 -	8.0 4.67	<del>ن</del> ۳ر			below	avation ormule,
-19	Oross av	+62.5 +5.5	0.0	-5.6			amount	ırds exc noidal fa
·a	lo sulsV	70.0 13.2	0.0	900			luct	ic ya prisn
<b>4</b> d	Right De	+34.0	0.0	-11.2 -95.0		•	Dec	Sy Cub
·ď	Center D	+80.0 +8.8	0.0	-5.6				
.dı	Left Dep	+56.0 +4.2	O.O	0.0	•	,		•
·qı	Len. of en			80 2				
.53	Len. of ex	8	15					
	Station.	0-		64				

## SECOND METHOD OF OBTAINING THE SOLID CONTENTS.

In obtaining the solid contents by the second method, the actual end depths are used instead of the total depths. When the latter have been obtained by Rule II., the value of m is subtracted therefrom in order to obtain the former. The contents of the central part of the excavation or embankment are then obtained separately from those of the slopes.

RULE V. The contents of the slopes are obtained according to the directions given in Rule III., using the actual depths, instead of the total depths as there directed.

The true depth of the central portion is found by averaging the end depths. Its contents both in excavation and embankment are first found from Table 3, or its supplement, for a width of 10 feet, and at the end of each section, their sum is multiplied by a multiplier which will give the contents for the actual width. This multiplier is equal to one tenth of the width of road bed used.

For a	width	of 14	feet	the multiplier	is	1.4
66	"	15	"	"	•••••	1.5
46	46	16	46	46	*************	1.6
66	LE	20	46	66	***************	2.0
46	. "	22	44	44	••••••	2.2
66	46	24	"	66	•	2.4

In calculating by this method, the contents of the central portion of the excavation or embankment must be kept separate from the contents of the slopes throughout each section. And in order to avoid adding the corrections in each instance to the quantities for the slopes, it is better to place them also in separate columns.

To find the contents for the central portion for lengths of 100 feet, we have the following rule:

RULE VI. Take from Table 3 the amount opposite the average of the end depths, placing the amounts for exca-

vation and embankment in separate colums; and at the end of the section multiply their sum by the proper multiplier as before directed.

When the length of the mass is less than 100 feet, the supplement to Table 3, which is made out for all depths less than 20 feet, is to be used in the same manner as the supplements to Tables 4 and 5 (see the explanations under Rule III.) The next page contains examples of this mode of calculating quantities, in which the widths of road bed and slopes are the same as those in the examples before given.

If the cross section is irregular, that is, if the surface line A D or D E (Fig. 1) is not straight, the end depth may be obtained thus: If we suppose A F and H E to be the actual slopes, and designate the actual end area plus the area F B H by a, and designate by A that area which for a slope of 2 to 1 would give the same total depth as the former, (s representing the actual slope used) we shall have

a: A:: s: 2  
hence, 
$$A = \frac{2a}{s}$$

we shall have, then, the following rule:

RULE VII. If the cross section is irregular, calculate the true end area for the slope used, to which add the area of the triangle F B H, (Fig. 1) of which m is the altitude, and the width of road bed the base.

Multiply the sum of these areas by 2, and divide the product by the value of s used. Apply the result to Table 1 from which will be found the total depth. But if the solid contents are calculated by the second method given, the value of m must be subtracted from this total depth, in order to find the actual depth.

In taking estimates during the progress of the work, after summing up at the end of each section, the amounts (as given by the tables) which are *done*, they will be multiplied by the proper multipliers, as before directed, in order to obtain the actual number of cubic yards. And if the

ENT.	Correction of the correction o	•		1.21 1826.77	1827.98 7972.81	9800.79
EMBANKMENT	-saqo[S			3.63 7969.18	977.03 7972.81	
EWI	Central smairq			5.18 971.85		
ON.	Corrections for sor salopes.	2351.11	1.00	,	2354.12 9909.52	2263.64
EXCAVATION	Slopes.	9900.83	2.89	,	225.04 9909.52	
EX(	Central prisms.	1211.11	4.63	,	1225.04	
-AT	Length s	55.2 +32.7	+2.55	-2.8 -32.8		
	Depths.	55.5	5.1	5.6		
18	True Er	+60.3	0.0	-5.6		
-19	Cross av	+62.5	0.0	-5.6		
•.2	To sulaV	70.0		0.0		
•10	Right De	+34.0	0.0	-11.2		
·de	Center De	+80.0 +8.8	0.0	-5.6		
·41	Left Dep	+56.0	0.0	0.0		
	Length.	8	15	80 0		
	Station.	0 -		Ci	•	

 $1225.04 \times 2$  = 2450.08  $12263.64 \times .5 = 6131.82$ 

 $977.03 \times 1.4 = 1367.84$  $9800.79 \times$  .6 = 5880.47

Cubic yards Exc.=8581.90 Cubic yards emb. = 7248.31 By prismoidal formula = 8580.35 By prismoidal formula = 7248.32

3

second method of finding the solid contents is used, care must be taken to keep the amounts contained in the central part of the road, separate from those contained in the slopes.

Several tables of level cuttings, for each half foot in depth, designed for use in approximate estimates, are given on pages 114-117; the length of the stations being 100 feet, and the contents being given in cubic yards.

The contents, in cubic yards, of the solids to be deducted as directed in Rule IV., for various lengths, and for the same widths and slopes as the tables last mentioned, are given on pages 118 and 119.

#### DEMONSTRATION REFERRED TO ON PAGE 8.

Let l (Fig. 2) represent the depth at the left side.

" r " " " right side.

" c " " center.

The cross average will be  $=\frac{2c+!+r}{4}$ 

The area, taking the cross average as the depth, is  $= s \left(\frac{2c+r+l}{4}\right)^2$ , see Fig. 3 and Eq. 2.

The true area is  $=\frac{s(c \ l+c \ r)}{2}$ , see Eq. 1 and Fig. 2. The gain of area, then, by taking the cross average as the depth, will be  $s\left(\frac{2c+l+r}{4}\right)^2 - \frac{s(c \ l+c \ r)}{2}$ 

Reducing this, and representing this gain by G, we have  $G = \frac{s(4 c^2 - 4 c l - 4 c r + 2 l r + l^2 + r^2)}{16}$   $s(c - r + c - l)^2$ 

$$=\frac{s(c-r+c-l)^2}{16}$$

Designating the greater of these two differences c-r

and c—l by E, and the lesser difference by D; we have  $G = \frac{s(\pm E \pm D)^2}{16}$ .

It is evident that E or D may be either positive or negative, or =0, according as c is greater or less than r or l, or equal to them.

- 1. If both E and D are positive, that is, if the center depth is greater than each of the side depths, we have  $G = \frac{s(E+D)^2}{16}$
- 2. Or if both E and D are negative, (the centre depth being less than each of the side depths,) we shall have the same result.
- 3. If D=0, and E is positive, (the center depth being equal to one side depth, and greater than the other,) we have  $G=\frac{s E^2}{16}$
- 4. If D=0, and E is negative, (the centre depth being equal to one side depth, and less than the other,) we have, as in the third case,  $G = \frac{*E^2}{16}$
- 5. If E is positive and D negative, or if E is negative and D positive, (the center depth being greater than one of the side depths, and less than the other,) we have in either case  $G = \frac{s(E-D)^2}{16}$

In general, therefore, if the side depths are both greater or both less than the center depth, (cases 1 and 2) we have  $G = \frac{s(E+D)^2}{16}$ 

And in all other cases, (we include cases 3 and 4, together with case 5, for the sake of uniformity in the rule, it being immaterial when D=0, whether we prefix the sign plus or minus to it,) we have  $G = \frac{s(E-D)^2}{16}$ 

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Area.	D.	Depths.	Area.	D.
			2.0	7.80	.40
.05	.00	.01	.05	8.20	.41
0.1	.01	.02	2.1	8.61	.42
.15	.03	.03	.15	9.03	.43
0.2	.06	.04	2.2	9.46	.44
.25	.10	.05	.25	9.90	.45
0.3	.15	.06	2.3	10.35	.46
.35	.21	.07	.35	10.81	.47
0.4	.28	.08	2.4	11.28	.48
.45	.36	.09	.45	11.76	.49
0.5	.45	.10	2.5	12.25	.50
.55	.55	.11	.55	12.75	.51
-0.6	.66	.12	2.6	13.26	.52
.65	.78	.13	.65	13.78	.53
0.7	.91	.14	2.7	14.31	.54
.75	1.05	.15	.75	14.85	.55
0.8	1.20	.16	2.8	15.40	.56
.85	1.36	.17	.85	15.96	.57
0.9	1.53	.18	2.9	16.53	.58
.95	1.71	.19	.95	17.11	.59
1.0	1.90	.20	3.0	17.70	.60
.05	2.10	.21	•05	18.30	.61
1.1	2.31	.22	3.1	18.91	.62
.15	2.53	.23	.15	19.53	.63
1.2	2.76	.24	3.2	20.16	.64
.25	3.00	.25	.25	20.80	.65
1.3	3.25	.26	3.3	21.45	.66
.35	3.51	.27	.35	22.11	.67
1.4	3.78	.28	3.4	22.78	.68
.45	4.06	.29	.45	23.46	.69
1.5	4.35	.30	3.5	24.15	.70
.55	4.65	.31	.55	24.85	.71
1.6	4.96	.32	3.6	25.56	.72
.65	5.28	.33	.65	26.28	.73
1.7	5.61	.34	3.7	27.01	.74
.75	5.95	.35	.75	27.75	.75
1.8	6.30	.36	3 8	28.50	.76
.85	6.66	.37	.85	29.26	.77
1.9	7 03	.38	3.9	30.03	.78
.95	7.41	.39	.95	30.81	.79
	7.80	.40	1	31.60	.80

END AREAS.

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Areas.	<b>D</b> .	Depths.	Areas.	D.
4.0	31.60	.80	0.0	71.40	1.20
.05	32.40	.81	6.0	72.60	1.21
4.1	3 <b>3.</b> 21	.82	.05	73.81	1.22
.15	34.03	.83	6.1	75.03	1.23
4.2	34.86	.84	.15	76.26	1.24
.25	<sub>-</sub> 35.70	.85	6.2	77.50	1.25
4.3	36.55	.86	.25	78.75	1.26
.35	37.41	.87	6.3	80.01	1.27
4.4	38.28	.88	6.4	. 81.28	1.28
.45	39.16	.89	11 1	82.56	1.29
4.5	40.05	.90	.45 6.5	83.85	1.30
.55	40.95	.91	.55	85.15	1.31
4.6	41.86	.92	6.6	86.46	1.32
.65	42.78	.93	.65	87.78	1.33
4.7	43.71	.94	6.7	89.11	1.34
.75	44.65	.95	.75	90.45	1.35
4.8	45.60	.96	6.8	91.80	1.36
.85	46.56	.97	.85	93.16	1.37
4.9	47.53	.98	6,9	94.53	1.38
.95	48.51	.99	.95	95.91	1.39
5.0	49.50	1.00	7.0	97.30	1.40
.05	50.50	1.01	.05	98.70	1.41
5.1	51.51	1.02	7.1	100.11	1.42
.15	52.53	1.03	.15	101.53	1.43
5.2	53.56	1.04	7.2	102.96	1.44
.25	54.60	1.05	.25	104.40	1.45
5.3	55.65	1.06	7.3	105.85	1.46
.35	56.71 57.78	1.07	.35	107.31	1.47
5.4	58.86	1 08	7.4	108.78	1.48
.45	59.95	1.09	.45	110.26	1.49
5.5	61.05	1.10 1.11	7.5	111.75	1.50
.55	62.16	1.12	.55	113.25	1.51
<b>5.6</b>	63.28	1.13	7.6	114.76 116.28	1.52 1.53
.65	64.41	1.14	.65	117.81	1.54
5.7	65.55	1.15	7.7	117.81	1.55
.75	66.70	1.16	.75	120.90	1.56
5.8	67.86	1.17	7.8	122.46	1.57
.85	69.03	1.18	.85	124.03	1.58
5.9	70.21	1.19	7.9	125.61	1.59
.95	71.40	1.20	.95	127.20	1.60

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Areas.	D.	Depths.	Areas.	<b>D.</b>
8.0	127.20	1.60	10.0	199.00	2.00
.05	128.80	1.61	.05	201.00	2.01
8.1	130.41	1.62	10.1	203.01	2.02
.15	132.03	1.63	.15	205.03	2.03
8.2	133.66	1.64	10.2	207.06	2.04
	135.30	1.65		209.10	2.05
.25 8.3	136.95	1.66	.25 10.3	211.15	2.06
	138.61	1.67	]] = }	213.21	2.07
.35	140.28	1.68	.35	215.28	2.08
8.4	141.96	1.69	10.4	217.36	2.09
.45	143.65	1.70	.45	219.45	2.10
8.5	145.35	1.71	10.5	221.55	2.11
.55	147.06	1.72	.55	<b>223.66</b>	2.12
8.6	148.78	1.73	10.6	225.78	2.18
.65	150.51	1.74	.65	227.91	2.14
8.7	152.25	1.75	10.7	230.05	2.15
.75	154.00	1.76	.75	232.20	2.16
8.8	155.76	1.77	10.8	234.36	2.17
.85	157.53	1.78	.85	236.53	2.18
8.9	159.31	1.79	10.9	238.71	2.19
.95	161.10	1.80	.95	240.90	2.20
9.0	162.90	1.81	11.0	243.10	2.21
.05	164.71	1.62	.05	245.31	2.22
9.1	166.53	1.83	11.1	247.53	2.23
.15	168.36	1.84	.15	249.76	2.24
9.2	170.20	1.85	11.2	252.00	2.25
.25	170.20	1.86	.25	254.25	2.26
9.3	172.03	1.87	11.8	256.51	2.27
.35		1.88	.35	258.78	2.28
9.4	175.78	1.89	11.4	261.06	2.29
.45	177.66	1.90	.45	263.35	2.30
9.5	179.55		11.5	265.65	2.31
.55	181.45	1.91	.55	267.96	2.32
9.6	183.36	1.92	11.6	207.90 270.28	2.38
.65	185.28	1.93	.65	270.28 272.61	2.84
9.7	187.21	1.94	11.7	272.01 274.95	2.35
.75	189.15	1.95	.75	•	2.36
9.8	191.10	1.96	11.8	277.30	2.80 2.87
.85	193.06	1.97	.85	279.66	
9.9	195.03	1.98	11.9	282.03	2.38 2.39
.95	197.01	1.99	.95	284.41	
.00	199.00	2.00	u	286.80	2.40

#### END AREAS.

TABLE 1,-END AREAS-SLOPE 2 TO 1.

Depths.	Areas.	<b>D.</b>	Depths.	Areas.	D.
12.0	286.80	2.40	14.0	390.60	2.80
.05	289.20	2.41	.05	393.40	2.81
12.1	291.61	2.42	14.1	396.21	2.82
.15	294.03	2.43	.15	399.03	2.83
12.2	296.46	2.44	14.2	401.86	2.84
.25	298.90	2.45	.25	404.70	2.85
.25 12. <b>3</b>	301.35	2.46	14.3	407.55	2.86
.35	303.81	2.47	.35	410.41	2.87
.65 12.4	306.28	2.48	.35 14.4	413.28	2.88
.45	308.76	2.49	11	416.16	2.89
12.5	311.25	2.50	.45 14.5	419.05	2.90
.55	313.75	2.51	.55	421.95	2.91
.85 12.6	316.26	2.52	14.6	424.86	2.92
.65	318.78	2.53	.65	427.78	2.93
12.7	321.31	2.54	14.7	430.71	2.94
.75	323.85	2.55	.75	433.65	2.95
12.8	326.40	2.56	14.8	436.60	2.96
.85	328.96	2.57	.85	439.56	2.97
12.9	331.53	2.58	14.9	442.53	2.98
.95	334.11	2.59	.95	445.51	2.99
13.0	336.70	2.60	15.0	448.50	3.00
.05	339.30	2.61	.05	451.50	3.01
13.1	341.91	2.62	15.1	454.51	3.02
.15	344.53	2.63	.15	457.53	3.03
13.2	347.16	2.64	15.2	460.56	3.04
.25	349.80	2.65	.25	463.60	3.05
13.3	352.45	2.66	15.3	466.65	3.06
.35	355.11	2.67	.35	469.71	3.07
13.4	357.78	2.68	15.4	472.78	3.08
.45	360.46	2.69	.45	475.86	3.09
18.5	363.15	2.70	15.5	478.95	3.10
.55	365.85	2.71	.55	482.05	3.11
18.6	368.56	2.72	15.6	485.16	3.12
.65	371.28	2.73	.65	488.28	3.13
13.7	374.01	2.74	15.7	491.41	3.14
.75	376.75	2.75	.75	494.55	3.15
13.8	379.50	2.76	15.8	497.70	3.16
.85	382.26	2.77	.85	500.86	3.17
13.9	385.03	2.78	15.9	504.03	3.18
.95	387.81	2.79	.95	507.21	3.19
•	390.60	2.80	u	510.40	3.20

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Areas.	<b>D</b> .	D.pths.	Areus.	<b>D</b> .
16.0	510.40	3.20	180	646 20	3.60
.05	513.60	3.21	.05	649.80	3.61
16.1	516.81	3.22	18.1	653.41	3.62
.15	520.03	3.23	.15	657.03	3.63
16.2	523.26	3.24	18.2	660.66	3.64
.25	<b>526.50</b>	3.25	.25	664 30	3.65
16.3	<b>529.75</b>	3.26	18.3	667 95	3.66
.35	533.01	3.27	.35	671. <b>6</b> 1	3.67
16.4	<b>536.28</b>	3.28	18.4	6 <b>75.2</b> 8	3.68
.45	539.56	3.29	.45	678.96	3.69
16.5	542.85	3.30	18.5	682,65	3.70
.55	546.15	3.31	.55	686.35	3.71
16.6	<b>549.46</b>	3.32	18.6	690.06	3.72
.65	<b>552.78</b>	3.33	.65	693.78	3.73
16.7	556.11	3.34	18.7	697.51	3.74
.75	559.45	3.35	.75	701.25	3.75
16.8	<b>562.80</b>	3.36	18.8	705.00	3,76
.85	566.16	3.37	.85	708,76	3.77
16.9	569.53	3.38	18.9	712,53	3.78
.95	572.91	3.39	.95	716.31	3.79
17.0	576.30	3.40	19.0	720.10	3,80
.05	<b>579.70</b>	3.41	.05	723.90	3.81
17.1	583.11	3.42	19,1	727.71	3.82
.15	586.53	3.43	.15	731,53	3.83
17.2	589.96	3.44	19.2	735.36	3.84
.25	593.40	3.45	.25	739.20	3.85
17.8	596.85	3.46	19.3	743.05	3,86
.35	600.31	3.47	.35	746.91	3.87
17.4	603.78	3.48	19.4	750.78	3.88
.45	607.26	3.49	.45	754,66	3.89
17.5	610.75	3.50	19.5	758.55	3,90
.55	614.25	3.51	.55	762.45	3.91
17.6	617.76	3.52	19.6	766,36	3.92
.65	621.28	3.53	.65	770.28	<b>3.9</b> 3
17.7	624.81	3.54	19.7	774.21	3,94
.75	628.35	3.55	.75	778.15	3.95
17.8	631.90	3 56	19.8	782.10	3,96
.85	635.46	3.57	.85	<b>786.06</b> .	3.97
17.9	639.03	3.58	19.9	790,03	3.98
.95	642.61	3.59	.95	794.01	3.99
	646.20	3.60		798.00	4,00

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Areas.	D.	Depths.	Areas.	D.
20.0	798.00	4.00	22.0	965.80	4.40
.05	802.00	4.01	.05	970.20	4.41
20.1	806.01	4.02	22.1	974.61	4.42
.15	810.03	4.03	.15	979.03	4.43
20.2	814.06	4.04	22.2	983.46	4.44
	818.10	4.05	100000000000000000000000000000000000000	987.90	4.45
.25	822.15	4.06	.25	992.35	4.46
20.3	826.21	4.07	22.3	996.81	4.47
.35	830.28	4.08	.35	1001.28	4.48
20.4	834.36	4.09	22.4	1005.76	4.49
.45	838.45	4.10	.45	1010.25	4.50
20.5	842.55	4.11	22.5	1014.75	4.51
.55	846.66	4.12	.55	1019.26	4.52
20.6	850.78	4.13	22.6	1023.78	4.53
.65	854.91	4.14	.65	1028.31	4.54
20.7	859.05	4.15	22.7	1032.85	4.55
.75	863.20	4.16	.75	1037.40	4.56
20.8	867.36	4.17	22.8	1041.96	4.57
.85	871.53	4.18	.85	1046.53	4.58
20.9	875.71	4.19	22.9	1051 11	4.59
.95	879.90	4.20	.95	1055.70	4.60
21.0	884.10	4.21	23.0	1060.30	4.61
.05	888.31	4.22	.05	1064.91	4.62
21.1	892.53	4.23	23.1	1069.53	4.63
.15	896.76	4.24	.15	1074.16	4.64
21.2	COULD'S COULD	The second second	23.2	The Art I was a first and the	1977
.25	901.00	4.25	.25	1078.80	4.65
21.3	905.25	4.26	23.3	1083.45	4.66
.35	909.51	4.27	.35	1088.11	4.67
21.4	913.78	4.28	23.4	1092.78	4.68
.45	918.06	4 29	.45	1097.46	4.69
21.5	922.35	4.30	23.5	1102.15	4.70
.55	926.65	4.31	.55	1106.85	4.71
21.6	930.96	4 32	23.6	1111.56	4.72
.65	935.28	4.33	.65	1116.28	4.73
21.7	939.61	4.34	23.7	1121.01	4.74
.75	943.95	4.35	.75	1125.75	4.75
21.8	948.30	4.36	23.8	1130.50	4.76
.85	952.66	4.37	.85	1135.26	4.77
21.9	957.03	4.38	23.9	1140.03	4.78
.95	961.41	4.39	.95	1144.81	4.78
.95	965.80	4.40	.66.	1149.60	4.80

4

TABLE 1.—END AREAS—SLOPE 2 TO 1.

24.0       1154.40       4.81       26.0       1354.60       359.81         24.1       1164.03       4.83       26.1       1359.81       359.81         24.2       1164.03       4.83       1.5       1365.03       370.26       320.26         24.2       1173.70       4.85       26.2       1375.50       320.25       1380.75       320.26       325.25       1380.75       320.26       320.25       1380.75       320.26       320.25       1380.75       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26       320.26	5.20 5.21 5.22 5.23 5.24 5.25 5.26 5.27 5.28 5.29 5.30 5.31
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.22 5.23 5.24 5.25 5.26 5.27 5.28 5.29 5.30
24.1       1159.21       4.82       26.1       1359.81       3         .15       1164.03       4.83       .15       1365.03       3         24.2       1168.86       4.84       26.2       1370.26       3         .25       1173.70       4.85       26.2       1375.50       3         .24.3       1178.55       4.86       26.3       1380.75       3         .35       1183.41       4.87       .35       1386.01       3         .35       1188.28       4.88       26.4       1391.28       3         24.4       1193.16       4.89       26.4       1396.56       4         .45       1198.05       4.90       26.5       1407.15       4         .45       1202.95       4.91       .55       1407.15       4         .45       1202.95       4.91       .55       1407.15       4         .46       1212.78       4.93       26.5       1412.46       4         .47       1222.65       4.95       .75       1428.45       5         .47       1222.65       4.96       26.8       1439.16       8         .49       124.51	5.23 5.24 5.25 5.26 5.27 5.28 5.29 5.30
24.1         1164.03         4.83         20.1         15         1365.03         3           24.2         1173.70         4.85         26.2         1370.26         3           .25         1178.55         4.86         26.3         1380.75         3           .35         1188.28         4.88         26.3         1386.01         3           .35         1188.28         4.88         26.4         1391.28         3           .45         1193.16         4.89         .45         1396.56         3           .45         1198.05         4.90         26.5         1401.85         3           .45         1202.95         4.91         .55         1407.15         3           .55         1207.86         4.92         26.5         1407.15         3           .46         1212.78         4.93         .65         1412.46         3           .47         1222.65         4.95         .75         1428.45         3           .48         1237.53         4.98         26.8         1433.80         3           .49         .95         1247.50         5.00         27.0         1455.30         3	5.24 5.25 5.26 5.27 5.28 5.29 5.30
24.2       1168.86       4.84       26.2       1370.26       3         .25       1173.70       4.85       26.2       1375.50       3         .24.3       1185.55       4.86       26.3       1380.75       3         .35       1183.41       4.87       .35       1386.01       3         .34.4       1193.16       4.89       26.4       1391.28       3         .45       1198.05       4.90       26.5       1401.85       3         .45       1202.95       4.91       .55       1407.15       3         .46       1207.86       4.92       26.5       1401.85       4         .46       1212.78       4.93       26.5       1412.46       4         .47       1222.65       4.95       .65       1423.11       4       4         .47       1222.65       4.95       .75       1428.45       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4       4	5.25 5.26 5.27 5.28 5.29 5.30
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.26 5.27 5.28 5.29 5.30
24.3       1178.55       4.86       26.3       1380.75       35         24.4       1188.28       4.88       26.4       1391.28       35         24.4       1193.16       4.89       26.4       1396.56       36         24.5       1198.05       4.90       26.5       1401.85       36         24.5       1202.95       4.91       .55       1407.15       36         24.6       1212.78       4.93       26.6       1412.46       36         24.6       1212.78       4.93       65       1417.78       36         24.7       1222.65       4.95       .65       1423.11       37         24.7       1222.65       4.95       .75       1428.45       37         24.8       1237.50       4.96       26.8       1433.80       38         24.9       1242.51       4.99       26.9       1444.53       38         24.9       1242.51       4.99       .95       1449.91       38         25.0       1252.50       5.01       .05       1455.30       38         25.1       1262.53       5.03       .15       1476.96       38         25.2       1	5.27 5.28 5.29 5.30
.35         1183.41         4.87         .35         1386.01         35         1391.28         34.4         1391.28         1396.56         35         1396.56         35         1396.56         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36         36	5.28 5.29 5.30
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.29 5.30
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.30
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.21
24.6     1207.86     4.92     26.6     1412.46     3       .65     1212.78     4.93     .65     1417.78     3       24.7     1217.71     4.94     26.7     1423.11     3       24.7     1222.65     4.95     .75     1428.45     3       24.8     1232.56     4.97     26.8     1433.80     3       24.9     1237.53     4.98     26.9     1439.16     3       24.9     1242.51     4.99     .95     1444.53     3       25.0     1252.50     5.00     27.0     1455.30     3       25.1     1262.53     5.03     .05     1466.11     3       25.1     1262.53     5.03     .15     1476.96     3       25.2     1272.60     5.05     .25     1482.40     3       25.3     1282.71     5.07     .35     1493.31     3       .35     1287.78     5.08     27.4     1498.78     5       25.4     1292.86     5.09     27.4     1504.26     5	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.32
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.33
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.34
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.35
24.8     1232.56     4.97     26.8     1439.16     35       24.9     1242.51     4.99     26.9     1444.53     35       25.0     1247.50     5.00     27.0     1455.30     35       25.1     1257.51     5.02     27.1     1466.11     35       25.1     1262.53     5.03     .15     1471.53     35       25.2     1272.60     5.05     27.2     1476.96     35       25.3     1282.71     5.07     27.3     1482.40     35       25.3     1287.78     5.08     27.3     1493.31     35       25.4     1292.86     5.09     27.4     1498.78     35       25.4     1292.86     5.09     27.4     1504.26     55	5.36
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.37
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.38
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.39
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.40
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.41
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.42
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.43
25.2   1272.60   5.05   27.2   1482.40   5 25   1277.65   5.06   27.3   1487.85   5 25.3   1282.71   5.07   .35   1493.31   5 25.4   1292.86   5.09   27.4   1498.78   5 25.4   1292.86   5.09   27.4   1504.26   5	5.44
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.45
25.3   1282.71   5.07   27.3   1493.31   5 .35   1287.78   5.08   .35   1498.78   5 25.4   1292.86   5.09   27.4   1504.26   5	5.46
35 1287.78 5.08 35 1498.78 5 25.4 1292.86 5.09 27.4 1504.26 5	5.47
25.4 1999 86 5.09 27.4 1504.26 5	5.48
	5.49
.45 1907.05 5.10 .40 1509.75 5	5.50
25.5   1303 05   5.11   27.5   1515.25   5	5.51
.55   1308 16   5 12   .55   1520 76   5	5.52
25.6   1919 99   5.19   27.6   1596 98   5	5.53
.65   1318 41   5 14   .65   1531 81   5	5.54
25.7   1992 55   5.15   27.7   1537 35   5	5.55
.75   1328 70   5 16   .75   1542 90   5	5.56
25.8   1333 86   5.17   27.8   1548.46   5	5.57
.85   1339 03   5 18   .85   1554 03   5	5.58
25.9   1344 21   5 19   27.9   1559.61   5	5.59
VE TOTAL OF THE STATE OF THE ST	5.60

END AREAS.

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Areas.	D.	Depths.	Areas.	D.
28.0	1565.20	5.60	30.0	1797.00	6.00
.05	1570.80	5.61	.05	1803.00	6.01
28.1	1576.41	5.62	30.1	1809.01	6.02
.15	1582.03	5.63		1815.03	6.03
28.2	1587.66	5.64	.15	1821.06	6.04
.25	1593.30	5.65	30.2	1827.10	6.05
28.3	1598.95	5.66	.25	1833.15	6.06
.35	1604.61	5.67	30.3	1839.21	6.07
28.4	1610.28	5.68	.35	1845.28	6.08
	1615.96	5.69	30.4	1851.36	6.09
.45	1621.65	5.70	.45	1857.45	6.10
28.5	1627.35	5.71	30.5	1863.55	6.11
.55	1633.06	5.72	.55	1869.66	6.12
28.6	1638.78	5.73	30.6	1875.78	6.13
.65	1644.51	5.74	.65	1881.91	6.14
28.7	1650.25	5.75	30.7	1888.05	6.15
.75	1656.00	5.76	.75	1894.20	6.16
28.8	1661.76	5.77	30.8	1900.36	6.17
.85	1667.53	5.78	.85	1906.53	6.18
28.9	1673.31	5.79	30.9	1912.71	6.19
.95	1679.10	5.80	.95	1918.90	6.20
29.0	1684.90	5.81	31.0	1925.10	6.21
.05	1690.71	5.82	.05	1931.31	6.22
29.1	1696.53	5.83	31.1	1937.53	6.23
.15	1702.36	5.84	.15	1943.76	6.24
29.2	1708.20	5.85	31.2	1950.00	6.25
.25	1714.05	5.86	.25	1956.25	6.26
29.3	1719.91	5.87	31.3	1962.51	6.27
.35	1725.78	5.88	.35	1968.78	6.28
29.4	1731.66	5.89	31.4	1975.06	6.29
.45	1737.55	5.90	.45	1981.35	6.30
29.5	1743.45	5.91	31.5	1987.65	6.31
.55	1749.36	5.92	.55	1993.96	6.32
29.6	1755.28	5.93	31.6	2000.28	6.33
.65	1761.21	5.94	.65	2006.61	6.34
29.7	1767.15	5.95	31.7	2012.95	6.35
.75	1773.10	5.96	.75	2019.30	6.36
29.8	1779.06	5.97	31.8	2025.66	6.37
.85	1785.03	5.98	.85	2032.03	6.38
29.9	1791.01	5.99	31.9	2038.41	6.39
.95	1797.00	6.00	.95	2044.80	6.40
i	1101.00	0.00	1	~V22.0U	0.40

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Arcas.	D.	Depths.	Arcas.	D.
32.0	2044.80	6.40	34.0	2308.60	6.80
	2051.20	6.41	.05	2315.40	6.81
.05 32.1	2057.61	6.42	34.1	2322.21	6.89
	2064.03	6.43	.15	2329.03	6.83
.15	2070.46	6.44	34.2	2335.86	6.84
32.2	2076.90	6.45	.25	2342.70	6.85
.25 32.3	2083.35	6.46	34.3	2349.55	6.86
	2089.81	6.47	.35	2356.41	6.87
.35	2096.28	6.48	34.4	2363.28	6.88
32.4	2102.76	6.49	.45	2370.16	6.89
.45	2109.25	6.50		2377.05	6.90
32.5	2115.75	6.51	34.5	2383.95	6.91
.55	2122.26	6.52	.55	2390.86	6.92
32.6	2128.78	6.53	34.6	2397.78	6.93
.65	2135.31	6.54	.65	2404.71	6.94
32.7	2141.85	6.55	34.7	2411.65	6.95
.75	2148.40	6.56	.75	2418.60	6.96
32.8	2154.96	6.57	34.8	2425.56	6.97
.85	2161.53	6.58	.85	2432.53	6.98
32.9	2168.11	6.59	34.9	2439.51	6.99
.95	2174.70	6.60	.95	2446.50	7.00
33.0	2181.30	6.61	35.0	2453.50	7.01
.05	2187.91	6.62	.05	2460.51	7.02
33.1	2194.53	6.63	35.1	2467.53	7.03
.15	2201.16	6.64	.15	2474.56	7.04
33.2	2207.80	6.65	35.2	2481.60	7.05
.25	2214.45	6.66	.25	2488.65	7.06
33.3	2221.11	6.67	35.3	2495.71	7.07
.35	2227.78	6.68	.35	2502.78	7.08
33.4	2234.46	6.69	35.4	2509.86	7.09
.45	2241.15	6.70	.45	2516.95	7.10
33.5	2247.85	6.71	35.5	2524.05	7.11
.55	2254.56	6.72	.55	2531.16	7.12
33.6	2261.28	6.73	35.6	2538.28	7.13
.65	2268-01	6.74	.65	2545.41	7.14
33.7	2274.75	6.75	35.7	2552.55	7.15
.75	2281.50	6.76	.75	2559.70	7.16
33.8	2288.26	6.77	35.8	2566.86	7.17
.85	2295.03	6.78	.85	2574.03	7.18
33.9	2301.81	6.79	35.9	2581.21	7.19
.95	2308.60	6.80	.95	2588.40	7.20

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Areas.	D.	Depths.	Areas.	D.
36.0	2588.40	7.20	38.0	2884.20	7.60
.05	2595.60	7.21	.05	2891.80	7.61
36.1	2602.81	7.22	38.1	2899.41	7.62
.15	2610.03	7.23	.15	2907.03	7.63
36.2	2617.26	7.24	38.2	2914.66	7.64
.25	2624.50	7.25	.25	2922.30	7.65
36.3	2631.75	7.26	38.3	2929.95	7.66
.35	2639.01	7.27	.35	2937.61	7.67
36.4	2646.28	7.28	38.4	2945.28	7.68
.45	2653.56	7.29	.45	2952.96	7.69
36.5	2660.85	7.30	38.5	2960.65	7.70
.55	2668.15	7.31		2968.35	7.71
	2675.46	7.32	.55	2976.06	7.72
36.6	2682.78	7.33	38.6	2983.78	7.73
.65 36.7	2690.11	7.34	.65	2991.51	7.74
	2697.45	7.35	38.7	2999.25	7.75
.75	2704.80	7.36	.75	3007.00	7.76
36.8	2712.16	7.37	38.8	3014.76	7.77
.85	2719.53	7.38	.85	3022.53	7.78
36.9	2726.91	7.39	38.9	3030.31	7.79
.95	2734.30	7.40	.95	3038.10	7.80
37.0	2741.70	7.41	39.0	3045.90	7.81
.05	2749.11	7.42	.05	3053.71	7.82
37.1	2756.53	7.43	39.1	3061.53	7.83
.15	2763.96	7.44	.15	3069.36	7.84
37.2	2771.40	7.45	39.2	3077.20	7.85
.25	2778.85	7.46	.25	3085.05	7.86
27.3	2786.31	7.47	39.3	3092.91	7.87
.35	2793.78	7.48	.35	3100.78	7.88
37.4	2801.26	7.49	39,4	3108.66	7.89
.45	2808.75	7.50	.45	3116.55	7.90
37.5	2816.25	7.51	39.5	3124.45	7.91
.55	2823.76	7.52	.55	3132.36	7.92
37.6	2831.28	7.53	39.6	3140.28	7.93
.65	2838.81	7.54	.65	3148.21	7.94
37.7	2846.35	7.55	39.7	3156.15	7.95
.75	2853.90	7.56	.75	3164.10	7.96
37.8	2861.46	7.57	39.8	3172.06	7.97
.85	2869.03	7.58	.85	3180.03	7.98
37.9	2876.61	7.59	39.9	3188.01	7.99
.95	2884.20	7.60	.95	3196.00	8.00

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Arcas.	<b>D</b> .	Depths.	Areas.	D.
40.0	3196.00	8.00	42.0	3523.80	8.40
	3204.00	8.01	.05	<b>3532.20</b>	8.41
.05	3212.01	8.02	42.1	3540.61	8.42
40.1	3220.03	8.03	.15	<b>354</b> 9.03	8.43
.15	3228.06	8.04	42.2	3557.46	8.44
40.2	3236.10	8.05	i	3565.90	8.45
.25	3244.15	8.06	.25 42.3	3574.35	8.46
40.3	<b>3252.21</b>	8.07		3582.81	8.47
.35	3260.28	8.08	.35	· 3591.28	8.48
40.4	3268.36	8.09	42.4	3599.76	8.49
.45	3276.45	8.10	.45	3608.25	8.50
40.5	3284.55	8.11	42.5	3616.75	8.51
.55	3292.66	8.12	.55	<b>362</b> 5.26	8.52
40.6	3300.78	8.13	42.6	3633.78	8.53
.65	3308.91	8.14	.65	3642.31	8.54
40.7	3317.05	8.15	42.7	3650.85	8.55
.75	3325.20	8.16	.75	3659.40	8.56
40.8	3333.36	8.17	42.8	3667.96	8.57
.85	3341.53	8.18	.85	3676.53	8.58
40.9	3349.71	8.19	42.9	3685.11	8.59
.95	3357.90	8.20	.95	3693.70	8.60
41.0	3366.10	8.21	43.0	3702.30	8.61
.05	3374.31	8.22	.05	3710.91	8.62
41.1	3382.53	8.23	43.1	3719.53	8.63
.15	3390.76	8.24	.15	3728.16	8.64
41.2	3399.00	8.25	43.2	3736.80	8,65
.25	3407.25	8.26	.25	3745.45	8.66
41.3	3415.51	8.27	43.3	3754.11	8.67
.35	3423.78	8.28	.35	3762.78	8.68
41.4	3432.06	8.29	43.4	3771.46	8.69
.45	3440.35	8.30	.45	3780.15	8.70
41.5	3448.65	8.31	43.5	3788.85	8.71
.55	3456.96	8.32	.55	3797.56	8.72
41.6	3465.28	8.33	43.6	3806.28	8.73
.65	3473.61	8.34	.65	3815.01	8.74
41.7	3481.95	8.35	43.7	3823.75	8.75
.75	3490.30	8.36	.75	38 <b>3</b> 2.50	8.76
41.8	3498.66	8.37	43.8	3841.26	8.77
.85	3507.03	8.38	.85	3850.03	8.78
41.9	3515.41	8.39	43.9	3858.81	8.79
.95	3523.80	8.40	.95	3867.60	8.80
ī	3323.8U	0.40	ı (	9001.00	9.50

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Area.	<b>D</b> .	Depths.	Arca.	<b>D</b> .
44.0	3867.60	8.80	46.0	4227.40	9.20
.05	3876.40	8.81	.05	4236.60	9.21
44.1	3885.21	8.82	46.1	4245.81	9.22
.15	3894.03	8.83	.15	4255.03	9.23
44.2	3902.86	8.84	46.2	4264.26	9.24
	3911.70	8.85	.25	<b>4273</b> .50	9.25
.25 44.3	3920.55	8.86	46.3	4282.75	9.26
.35	3929.41	8.87	.35	4292.01	9.27
44.4	3938.28	8.88	46.4	4301.28	9.28
.45	3947.16	8.89	.45	4310.56	9.29
44.5	3956.05	8.90	46.5	4319.85	9.30
.55	3964.95	8.91	.55	4329.15	9.31
44.6	3973.86	8.92	46.6	4338.46	9.32
.65	3982.78	8.93	.65	4347.78	9.33
44.7	3991.71	8.94	46.7	4357.11	9.34
	4000.65	8.95	.75	4366.45	9.35
.75	4009.60	8.96	46.8	4375.80	9.36
44.8	4018.56	8.97	.85	4385.16	9.37
.85 44.9	4027.53	8.98	46.9	4394.53	9.38
	4036,51	8.99	.95	4403.91	9.39
.95	4045.50	9.00	47.0	4413.30	9.40
45.0	4054.50	9.01	.05	4422.70	9.41
.05	4063.51	9.02	47.1	4432.11	9.42
45.1	4072.53	9.03	.15	4441.53	9.43
.15 <b>45.2</b>	4081.56	9.04	47.2	4450.96	9.44
	4090.60	9.05	.25	4460.40	9.45
.25 45.3	4099.65	9.06	47.3	4469.85	9.46
	4108.71	9.07	.35	4479.31	9.47
.35	4117.78	9.08	47.4	4488.78	9.48
45.4	4126.86	9.09	.45	4498.26	9.49
.45 45.5	4135.95	9.10	47.5	4507.75	9.50
	· 4145.05	9.11	.55	4517.25	9.51
.55	4154.16	9.12	47.6	4526.76	9.52
45.6	4163.28	9.13	1	4536.28	9.53
.65	4172.41	9.14	.65 47.7	4545.81	9.54
45.7	4181.55	9.15	4	4555.35	9.55
.75	4190.70	9.16	.75 47.8	4564.90	9.56
45.8	4199.86	9.17	i i	4574.46	9.57
.85	4209.03	9.18	.85 47.9	4584.03	9.58
45.9	4218.21	9.19	.95	4593.61	9.59
.95	4227.40	9.20	.95	4603.20	9.60

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TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Areas.	<b>D</b> .	Depths.	Areas.	<b>D</b> .
48.0	4603.20	9.60	50.0	4995.00	10 00
	4612.80	9.61	.05	5005.00	10.01
.05	4622.41	9.62	50.1	5015.01	10.02
48.1	4632.03	9.63		5025.03	10.03
.15	4641.66	9.64	.15	5035.06	10.04
48.2	4651.30	9.65	50.2	5045.10	10.05
.25	4660.95	9.66	.25	5055.15	10.06
48.3	4670.61	9.67	50.3	5065.21	10.07
.35	4680.28	9.68	.35	5075.28	10.08
48.4	4689.96	9.69	50.4	5085.36	10.09
.45	4699.65	9.70	.45	5095.45	10.10
48.5	4709.35	9.71	50.5	5105.55	10.11
.55	4719.06	9.72	.55	5115.66	10.12
48.Ն	4728.78	9.73	50.6	5125.78	10.13
.65	4738.51	9.74	.65	5135.91	10.14
48.7	4748.25	9.75	50.7	5146.05	10.15
.75	4758.00	9.76	.75	5156.20	10.16
48.8	4767.76	9.77	50.8	5166.36	10.17
.85	4777.53	9.78	.85	5176.53	10.18
48.9	4787.31	9.79	50.9	5186.71	10.19
.95	4797.10	9.80	.95	5196.90	10.20
49.0	4806.90	9.81	51.0	5207.10	10.21
.05	4816.71	9.82	.05	5217.31	10.22
49.1	4826.53	9.83	51.1	5227.53	10.23
.15	4836.36	9.84	.15	5237.76	10.24
49.2	4846.20	9.85	51.2	5248.00	10.25
.25	4856.05	9.86	.25	5258.25	10.26
49.3	4865.91	9.87	51.3	5268.51	10.27
.35	4875.78	9.88	.35	5278.78	10.28
49.4	4885.66	9.89	51.4	5289.06	10.29
.45	4895.55	9.90	.45	5299.35	10.30
49.5	4905.45	9.91	51.5	5309.65	10.31
.55	4915.36	9.92	.55	5319.96	10.32
49.6	4925.28	9.93	51.6	5330.28	10.33
.65	4935.21	9.94	.65	5340.61	10.34
49.7	4945.15	9.95	51.7	5350.95	10.34
.75	4955.10	9.96	.75	5361.30	10.36
49.8	4965.06	9.97	51.8	5371.66	10.37
.85	4975.03	9.98	.85	5382.03	10.37
49.9	4985.01	9.99	51.9	5392.41	10.39
.95	4995.00	10.00	.95	5402.80	10.39

33 END AREAS.

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Areas.	<b>D</b> .	Depths.	Areas.	<b>D</b> .
52.0	5402.80	10.40	54.0	5826.60	10.80
.05	5413.20	10.41		5837.40	10.81
52.1	5423.61	10.42	.05 54.1	5848.21	10.82
.15	<b>5434</b> .03	10.43	1	5859.03	10.83
52.2	<b>5444.46</b>	10.44	.15	5869.86	10.84
	<b>5454</b> .90	10.45	54.2	5880.70	10.85
.25	<b>546</b> 5.35	10.46	.25	5891.55	10.86
52.3	5475.81	10.47	54.3	5902.41	10.87
.35	5486.28	10.48	.35	5913.28	10.88
52.4	5496.76	10.49	54.4	5924.16	10.89
.45	5507.25	10.50	.45	5935.05	10.90
52.5	5517.75	10.51	54.5	5945.95	10.91
.55	5528.26	10.52	.55	5956.86	10.92
<b>52.6</b>	5538.78	10.53	54.6	5967.78	10.93
.65	5549.31	10.54	.65	5978.71	10.94
52.7	5559.85	10.55	54.7	5989.65	10.95
.75	5570.40	10.56	.75	6000.60	10.96
<b>52.8</b>	5580.96	10.57	54.8	6011.56	10.97
.85	5591.53	10.58	.85	6022.53	10.98
52.9	5602.11	10.59	54.9	6033.51	10.99
.95	5612.70	10.59	.95	6044.50	11.00
53.0	5623.30	10.61	55.0	6055.50	11.00
.05	-		.05		
53.1	5633.91	10.62	55.1	6066.51	11.02
.15	5644.53	10.63	.15	6077.53	11.03
53.2	5655.16	10.64	55.2	6088.56	11.04
.25	5665.80	10.65	.25	6099.60	11.0
53.3	5676.45	10.66	55.3	6110.65	11.06
.35	5687.11	10.67	.35	6121.71	11.07
53.4	5697.78	10.68	55.4	6132.78	11.08
.45	5708.46	10.69	.45	6143.86	11.09
53.5	5719.15	10.70	55.5	6154.95	11.10
.55	5729.85	10.71	.55	6166.05	11.13
53.6	<b>574</b> 0.56	10.72	55.6	6177.16	11.12
.65	5751.28	10.73	.65	6188.28	11.18
53.7	5762.01	10.74	55.7	6199.41	11.14
.75	<b>5772</b> .75	10.75	.75	6210.55	11.13
53.8	<b>5783</b> .50	10.76		6221.70	11.10
	<b>5794.26</b>	10.77	55.8	6232.86	11.1
.85	5805.03	10.78	.85	6244.03	11.1
53.9	5815.81	10.79	55.9	6255.21	11.19
.95	5826.60	10.80	.95	6266.40	11.20

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Areas.	D.	Depths.	Areas.	D.
56.0	6266.40	11.20	58.0	6722.20	11.60
.05	6277.60	11.21	.05	6733.80	11.61
56.1	6288.81	11.22	58.1	6745.41	11.62
	6300.03	11.23	.15	<b>67</b> 57.03	11.63
.15	6311.26	11.24	58.2	6768.66	11.64
56.2	6322.50	11.25		6780.30	11.65
.25	6333.75	11.26	.25	6791.95	11.66
56.3	6345.01	11.27	58.3	6803.61	11.67
.35	6356.28	11.28	.35	6815.28	11.68
56.4	6367.56	11.29	58.4	6826.96	11.69
.45	6378.85	11.30	.45	6838.65	11.70
56.5	6390.15	11.31	58.5	6850.35	11.71
.55	6401.46	11.32	.55	6862.06	11.72
56.6	6412.78	11.33	58.6	6873.78	11.73
.65	6424.11	11.34	.65	6885.51	11.74
56.7	6435.45	11.35	58.7	6897.25	11.75
.75	<b>644</b> 6.80	11.36	.75	6909.00	11.76
56.8	6458.16	11.37	58.8	6920.76	11.77
.85	6469.53	11.38	.85	6932.53	11.78
56.9	6480.91	11.39	58.9	6944.31	11.79
.95	6492.30	11.39	.95	6956.10	11.79
57.0			59.0	6967.90	
.05	6503.70	11.41	.05		11.81
57.1	6515.11	11.42	59.1	6979.71	11.82
.15	6526.53	11.43	.15	6991.53	11.83
57.2	6537.96	11.44	59.2	7003.36	11.84
.25	6549.40	11.45	.25	7015.20	11.85
57.3	6560.85	11.46	59.3	7027.05	11.86
.35	6572.31	11.47	.35	7038.91	11.87
57.4	<b>6583.7</b> 8	11.48	59.4	7050.78	11.88
.45	<b>6595.26</b> ,	11.49	.45	7062.66	11.89
57.5	6606.75	11.50	59.5	7074.55	11.90
.55	6618.25	11.51	.55	7086.45	11,91
	6629.76	11.52	59.6	7098.36	11.92
57.6	6641.28	11.53	.65	7110.28	11.93
.65	<b>6652.81</b>	11.54		7122.21	11.94
57.7	6664.35	11.55	59.7	7134.15	11.95
.75	6675.90	11.56	.75	7146.10	11.96
57.8	6687.46	11.57	59.8	7158 06	11.97
.85	6699.03	11.58	.85	7170.03	11.98
<b>57</b> .9	6710.61	11.59	59.9	7182.01	11.99
.95	6722.20	11.60	.95	7194.00	12.00

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Area.	D.	Depths.	Area.	D.
60.0	7194.00	12.00	62.0	7681.80	12.40
.05	7206.00	12.01	.05	7694.20	12.4
60.1	7218.01	12.02	62.1	7706.61	12.4
.15	7230.03	12.03	0.21	7719.03	12.4
60.2	7242.06	12.04	62.2	7731.46	12.4
.25	7254.10	12.05	.25	7743.90	12.4
60.3	7266.15	12.06	62.3	7756.35	12.4
.35	7278.21	12.07	25/6/6	7768.81	12.4
60.4	7290.28	12.08	.35	7781.28	12.4
20.00	7302.36	12.09	62.4	7793.76	12.49
.45	7314.45	12.10	.45	7806.25	12.5
60.5	7326.55	12.11	62.5	7818.75	12.5
.55	7338.66	12.12	.55	7831.26	12.5
60.6	7350.78	12.13	62.6	7843.78	12.5
.65	7362.91	12.14	.65	7856.31	12.5
60.7	7375.05	12.15	62.7	7868.85	12.5
.75	7387.20	12.16	.75	7881.40	12.5
60.8	7399.36	12.17	62.8	7893.96	12.5
.85	7411.53	12.18	.85	7906.53	12.5
60.9	7423.71	12.19	62.9	7919.11	12.5
.95	7435.90	12.20	.95	7931.70	12.6
61.0	7448.10	12.21	63.0	7944.30	12.6
.05	7460.31	12.22	.05	7956.91	12.6
61.1	7472.53	12.23	63.1	7969.53	12.6
.15	7484.76	12.24	.15	7982.16	12.6
61.2	7497.00	12.25	63.2	7994.80	12.6
.25	7509.25	12.26	.25	8007.45	12.6
61.3	7521.51	12.27	63.3	8020.11	12.6
.35	7533.78	12.28	.35	8032.78	12.6
61.4	7546.06	12.29	63.4	8045.46	12.6
.45	7558.35	12.30	.45	8058.15	12.7
61.5	7570.65	12.31	63.5	8070.85	12.7
.55	7582.96	12.32	.55	8083.56	12.7
61.6	7595.28	12.33	63.6	8096.28	12.7
.65	7607.61	12.34	.65	8109.01	12.7
61.7	7619.95	12.35	63.7	8121.75	12.7
.75	7632.30	12.36	.75	8134.50	
61.8	7644.66	12.36	63.8	8147.26	12.7
.85			.85	8160.03	12.7
61.9	7657.03	12.38	63.9		12.7
.95	7669.41	12.39	.95	8172.81	12.7
100	7681.80	12.40	122	8185.60	12.8

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Arcas.	D.	Depths.	Areas.	D.
64.0	8185.60	12.80	66.0	8705.40	13.20
	8198.40	12.81	.05	8718.60	13.21
.05	8211.21	12.82	66.1	8731.81	13.22
64.1	8224.03	12.83	.15	8745.03	13.23
.15	8236.86	12.84	66.2	8758.26	13.24
64.2	8249.70	12.85	.25	8771.50	13.25
.25	8262.55	12.86	66.3	8784.75	13.26
64.3	8275.41	12.87	.35	8798.01	13.27
.35	8288.28	12.88		8811.28	13.28
64.4	8301.16	12.89	66.4	8824.56	13.29
.45	8314.05	12.90	.45	8837.85	13.30
64.5	8326.95	12.91	66.5	8851.15	13.31
.55	8339.86	12.92	.55	8864.46	13.32
64.6	8352.78	12.93	66.6	8877.78	13.33
.65	8365.71	12.94	.65	8891.11	13.34
64.7	8378.65	12.95	66.7	8904.45	13.35
.75	8391.60	12.96	.75	8917.80	13.36
64.8	8404.56	12.97	66.8	8931.16	13,37
.85	8417.53	12.98	.85	8944.53	13.38
64.9	8430.51	12.99	66.9	8957.91	13.39
.95	8443.50	13.00	.95	8971.30	13.40
65.0	8456.50	13.01	67.0	8984.70	13,41
.05	8469.51	13.02	.05	8998.11	13,42
65.1	8482.53	13.03	67.1	9011.53	13.43
.15	8495.56	13.04	.15	9024.96	13,44
65.2	8508.60	13.05	67.2	9038.40	13.45
.25	8521.65	13.06	.25	9051.85	13.46
65.3	8534.71	13.07	67.3	9065.31	13.47
.35	8547.78	13.08	.35	9078.78	13.48
65.4	8560.86	13.09	67.4	9092.26	13.49
.45	8573.95	13.10	.45	9105.75	13.50
65.5	8587.05	13.11	67.5	9119.25	13.51
.55	8600.16	13.12	.55	9132.76	13.52
65.6	8613.28	13.13	67.6	9146.28	13.53
.65	8626.41	13.14	.65	9159.81	13.54
65.7	8639.55	13.15	67.7	9173.35	13.55
.75	8652.70	13.16	.75	9186.90	13.56
65.8	8665.86	13.17	67.8	9200.46	13.57
.85	8679.03	13.18	.85	9214.03	13.58
65.9	8692.21	13.19	67.9	9227.61	13.59
.95	8705.40	13.20	.95	9241.20	13.60
j	0700.40	19.20		3641.60	.0.00

## END AREAS.

TABLE 1.—END AREAS—SLOPE 2 TO 1.

Depths.	Areas.	D.	Depths.	Areas.	D.
68.0	9241.20	13.60	70.0	9793.00	14.00
The second secon	9254.80	13.61	.05	9807.00	14.01
.05 68.1	9268.41	13.62	70.1	9821.01	14.02
	9282.03	13.63	.15	9835.03	14.03
.15 68.2	9295.66	13.64	70.2	9849.06	14.04
.25	9309.30	13.65	.25	9863.10	14.05
68.3	9322.95	13.66	70.3	9877.15	14.06
.35	9336.61	13.67	.35	9891.21	14.07
68.4	9350.28	13.68		9905.28	14.08
	9363.96	13.69	70.4	9919.36	14.09
.45	9377.65	13.70	.45	9933.45	14.10
68.5	9391.35	13.71	70.5	9947.55	14.11
.55	\9405.06	13.72	.55	9961.66	14.12
68.6	9418.78	13.73	70.6	9975.78	14.13
.65	9432.51	13.74	.65	9989.91	14.14
68.7	9446.25	13.75	70.7	10004.05	14.15
.75	9460.00	13.76	.75	10018.20	14.16
68.8	9473.76	13.77	70.8	10032.36	14.17
.85	9487.53	13.78	.85	10046.53	14.18
68.9	9501.31	13.79	70.9	10060.71	14.19
.95	9515.10	13.80	.95	10074.90	14.20
69.0	9528.90	13.81	71.0	10089.10	14.21
.05	9542.71	13.82	.05	10103.31	14.22
69.1	9556.53	13.83	71.1	10117.53	14.23
.15	9570.36	13.84	.15	10131.76	14.24
69.2	9584.20	13.85	71.2	10146.00	14.25
.25	9598.05	13.86	.25	10160.25	14.26
69.3	9611.91	13.87	71.3	10174.51	14.27
.35	9625.78	13.88	.35	10188.78	14.28
69.4	9639.66	13.89	71.4	10203.06	14.29
.45	9653.55	13.90	.45	10217.35	14.30
69.5	9667.45	13.91	71.5	10231.65	14.31
.55	9681.36	13.92	.55	10245.96	14.32
69.6	9695.28	13.93	71.6	10260.28	14.33
.65	9709.21	13.94	.65	10274.61	14.34
69.7	9723.15	13.95	71.7	10288.95	14.35
.75	9737.10	13.96	.75	10303.30	14.36
69.8	9751.06	13.97	71.8	10317.66	14.37
.85	9765.03	13.98	.85	10332.03	14.38
69.9		13.99	71.9	10346.41	14.39
.95	9779.01	The second secon	.95	10340.41	
	9793.00	14.00	1	10900.00	14.40

Table 2.—Corrections for Cross Average—slope 2 to 1.

	v <sup>2</sup>	1	v <sup>2</sup>	l ago asy	v <sup>2</sup>
$oldsymbol{v}$		v		v	l —
	8		8		8
	İ	4.0	2.00	8.0	8.00
0.1	.00	.1	2.10	.1	8.20
.2	.00	.2	2.20	.2	8.40
.3	.01	.3	2.31	.3	8.61
.4	.02	.4	2.42	.4	8.82
.5	.03	.5	2.53	.5	9.03
.6	.05	.6	2.65	.6	9.25
.7	.06	.7	2.76	.7	9.46
.8	.08	.8	2.88	.8	9.68
.9	.10	.9	3.00	.9	9.90
1.0	.12	5.0	3.12	9.0	10.12
.1	.15	.1	3.25	.1	10.35
.2	.18	.2	3.38	.2	10.58
.3	.21	.3	3.51	.3	10.81
.4	.25	.4	3.65	.4	11.05
.5	.28	.5	3.78	.5	11.28
.6	.32	.6	3.92	.6	11.52
.7	.36	.7	4.06	.7	11.76
.8	.40	.8	4.20	.8	12.00
.9	.45	.9	4.35	.9	12.25
2.0	.50	6.0	4.50	10.0	12.50
.1	.55	.1	4.65	.1	12.75
.2	.61	.2	4.81	.2	13.01
.3	.66	.3	4.96	.3	13.26
.4	.72	.4	5.12	.4	13.52
.5	.78	.5	5.28	.5	13.78
.6	.84	.6	5.44	.6	14.04
.7	.91	.7	5.61	.7	14.31
.8	.98	.8	5.78	.8	14.58
.9	1.05	.9	5.95	.9	14.85
3.0	1.13	7.0	6.13	11.0	15.13
.1	1.20	.1	6.30	.1	15.40
.2	1.28	.2	6.48	.2	15.68
.3	1.36	.3	6 66	.3	15.96
.4	1.44	.4	6.84	.4	16.24
.5	1.53	.5	7.03	.5	16.53
.6	1.62	.6	7.22	.6	16.82
.7	1.71	.7	7.41	.7	17.11
.8	1.81	.8	7.61	.8	17.41
.9	1.90	.9	7.80	.9	17.70

Table 2.—Corrections for Cross Average—Slope 2 to 1.

		<del>, , , , , , , , , , , , , , , , , , , </del>			
	v2		v 2		v <sup>2</sup>
v	8	v	8	$oxed{v}$	8
12.0	18.00	16.0	32.00	20.0	50.00
.1	18.30	.1	32.40	.1	50.50
.2	18.60	.2	32.80	.2	51.00
.3	18.91	.3	33.21	.3	51.51
.4	19.22	.4	33.62	.4	52.02
.5	19.53	.5	34.03	.5	52.53
.6	19.85	.6	34.45	.6	53.05
.7	20.16	.7	34.86	.7	53.56
.8	20.48	.8	35.28	.8	54.08
.9	20.80	.9	35.70	.9	54.60
13.0	21.12	17.0	36.12	21.0	55.12
.1	21.45	.1	36.55	.1	55.65
.2	21.78	.2	36.98	.2	56.18
.3	22.11	.3	37.41	.3	56.71
.4	22.45	.4	37.85	.4	57.25
.5	22.78	.5	38.28	.5	57.78
.6	23.12	.6	38.72	.6	58.32
.7	23.46	.7	39.16	.7	58.86
.8	23.80	.8	39.60	8	59.40
.9	24.15	.9	40.05	.9	<b>59</b> .95
14.0	24.50	18.0	40.50	22.0	60.50
.1	24.85	.1	40.95	.1	61.05
.2	25.21	.2	41.41	.2	61.61
.3	25.56	.3	41.86	.3	62.16
.4	25.92	.4	42.32	.4	62.72
.5	26.28	.5	42.78	.5	63.28
.6	26.64	.6	43.24	.6	63.84
.7	27.01	.7	43.71	.7	64.41
.8	27.38	.8	44.18	.8	64.98
.9	27.75	.9	44.65	.9	65.55
15.0	28.13	19'0	45.13	23.0	66.13
.1	28.50	.1	45.60	.1	66.70
.2	28.88	.2	46.08	.2	67.28
.3	29.26	.3	46.56	.3	67.86
.4	29.64	.4	47.04	.4	68.44
.5	30.03	.5	47.53	.5	69.03
.6	30.42	.6	48.02	.6	69.62
.7	30.81	.7	48.51	.7	70.21
.8	31.21	.8	49.01	.8	70.81
.9	31.60	.9	49.50	.9	71.40

Table 2.—Corrections for Cross Average—Slope 2 to 1.

				-61	
	v <sup>2</sup>		v <sup>3</sup>		v <sup>2</sup>
$oldsymbol{v}$	8	v	8	v	8
24.0	72.00	27 0	91.13	30.0	112.50
.1	72.60	.1	91.80	.1	113.25
.2	73.20	.2	92.48	.2	114.01
.3	73.81	.3	93.16	.3	114.76
.4	74.42	.4	93.84	.4	115.52
.5	75.03	.5	94.53	.5	116.28
.6	75.65	.6	95.22	.6	117.04
.7	76.26	.7	95.91	.7	117.81
.8	76.88	.8	96.61	.8	118.58
.9	77.50	.9	97.30	.9	119.35
<b>25.0</b>	78.12	28.0	98.00	31.0	120.13
.1	78.75	.1	98.70	.1	120.90
.2	79.38	.2	99.40	.2	121.68
.3	80.01	.3	100.11	.3	122.46
.4	80.65	.4	100.82	.4	123.24
.5	81.28	.5	101.53	.5	124.03
.6	81.92	.6	102.25	.6	124.82
.7	82.56	.7	102.96	.7	125.61
.8	83.20	.8	103.68	.8	126.41
.9	83.85	.9	104.40	.9	127.20
<b>26.0</b>	84.50	29.0	105.12	,	
.1	85.15	.1	105.85		
.2	85.81	.2	106.58		
.3	86.46	.3	107.31	ł	
.4	87.12	.4	108.05		
.5	87.78	.5	108.78		
.6	88.44	.6	109.52		
.7	89.11	.7	110.26		
.8	89.78	.8	111.00		
.9	90.45	.9	111.75		

Table 3.—Contents of Prisms 10 ft. wide and 100 ft. long.

Depths.	Contents.	Depths.	Contents.
		4.0	148.1
0.1	3.70	.1	151.88
.2	7.41	.2	155.50
.3	11.11	.3	159.20
.4	14.81	.4	162.9
.5	18.52	.5	166.6
.6	22.22	.6	170.3
.7	25.93	.7	174.0
.8	29.63	.8	177.7
.9	33.33	.9	181.4
1.0	37.04	5.0	185.1
.1	40.74	.1	188.89
.2	44.44	.2	192.5
.3	48.15	.3	196.3
.4	51.85	.4	200.0
.5	55.56	.5	203.7
.6	59.26	.6	207.4
.7	62.96	.7	211.1
.8	66.67	.8	214.8
.9	70.37	.9	218.5
2.0	74.07	6.0	222.2
.1	77.78	.1	225.9
.2	81.48	.2	229.6
.3	85.19	.3	233.3
.4	88.89	.4	237.0
.5	92.59	.5	240.7
.6	96.30	.6	244.4
.7	100.00	.7	248.1
.8	103.70	.8	251.8
.9	107.41	.9	255.5
3.0	111.11	7.0	259.2
.1	114.81	.1	262.9
.2	118.52	.2	266.6
.3	122.22	.3	270.3
.4	125.93	.4	274.0
.5	129.63	.5	277.7
.6	133.33	.6	281.4
.7	137.04	.7	<b>285</b> .1
.8	140.74	.8	288.8
.9	144.44	.9	<b>292.5</b>

Table 3.—Contents of Prisms 10 ft. wide and 100 ft. long.

Depths.	Contents.	Depths.	Contents.
8.0	296.30	12.0	444.44
.1	300.00	.1	448.15
.2	303.70	.2	451.85
.3	307.41	.3	455.56
.4	311.11	.4	459.26
.5	314.81	.5	462.96
.6	318.52	.6	466.67
.7	322.22	.7	470.37
.8	325.93	.8	474.07
.9	329.63	.9	477.78
9.0	333.33	13.0	481.48
.1	337.04	.1	485.19
.2	340.74	.2	488.89
.3	344.44	.3	492.59
.4	348.15	.4	496.30
.5	351.85	.5	500.00
.6	355.56	.6	503.70
.7	359.26	.7	507.41
.8	362.96	.8	511.11
.9	366,67	.9	514.81
0.0	370,37	14.0	518.52
.1	374.07	.1	522.22
.2	377.78	.2	525.93
.3	381,48	.3	529.63
.4	385.19	.4	533.33
.5	388.89	.5	537.04
.6	392,59	.6	540.74
.7	396.30	.7	544.44
.8	400.00	.8	548.15
.9	403,70	.9	551.85
11.0	407.41	15.0	555.56
.1	411.11	.1	559.26
.2	414.81	.2	562.96
.3	418.52	.3	566.67
.4	422.22	.4	570.37
.5	425.93	.5	574.07
.6	429.63	.6	577.78
.7	433.33	.7	581.48
.8	437.04	.8	585.19
.9	440.74	.9	588.89

Table 3.—Contents of Prisms 10 ft. wide and 100 ft. long.

Depths.	Contents.	Depths.	Contents.
16.0	592.59	20.0	740.74
.1	596.30	.1	744.44
.2	600.00	.2	748.15
.3	603.70	.3	751.85
.4	607.41	.4	755.56
.5	611.11	.5	759.26
.6	614.81	.6	762.96
.7	618.52	.7	766.67
.8	622.22	.8	770.37
.9	625.93	.9	774.07
17.0	629.63	21.0	777.78
.1	633.33	.1	781.48
.2	637.04	.2	785.19
.3	640.74	.3	788.89
.4	644.44	.4	792.59
.5	648.15	.5	796.30
.6	651.85	-6	800.00
.7	655.56	.7	803.70
.8	659.26	-8	807.41
.9	662.96	.9	811.11
18.0	666.67	22.0	814.81
.1	670.37	-1	818.52
.2	674.07	.2	822.22
.3	677.78	-3	825.93
.4	681.48	.4	829.63
.5	685.19	-5	833.33
.6	688.89	-6	837.04
.7	692.59	.7	840.74
.8	696.30	-8	844.44
.9	700.00	.9	848.15
19.0	703.70	23.0	851.85
.1	707.41	-1	855.56
.2	711.11	.2	859.26
.3	714.81	-3	862.96
.4	718.52	.4	866.67
.5	722.22	-5	870.37
.6	725.93	-6	874.07
.7	729.63	.7	877.78
.8	733.33	.8	881.48
.9	737.04	.9	885.19

Table 3.—Contents of Prisms 10 ft. wide and 100 ft. long.

Depths.	Contents.	Depths.	Contents.
24.0	888.89	28.0	1037.04
.1	892.59	.1	1040.74
.2	896.30	.2	1044.44
.3	900.00	.3	1048.13
.4	903.70	.4	1051.85
.5	907.41	.5	1055.56
.6	911.11	.6	1059.26
.7	914.81	.7	1062.96
.8	918.52	.8	1066.67
.9	922.22	.9	1070.37
25.0	925.93	29.0	1074.07
.1	929.63	.1	1077.78
.2	933.33	.2	1081.48
.3	937.04	.3	1085.19
.4	940.74	.4	1088-89
.5	944.44	-5	1092.59
.6	948.15	-6	1096.30
.7	951.85	.7	1100.00
.8	955.56	-8	1103.70
.9	959.26	.9	1107.41
26.0	962.96	30.0	1111-11
.1	966.67	-1	1114.81
.2	970.37	.2	1118.52
.3	974.07	-3	1122-22
.4	977.78	.4	1125.98
.5	981.48	-5	1129.63
.6	985.19	-6	1133.33
.7	988.89	.7	1137.04
.8	992.59	-8	1140.74
9	996.30	.9	1144.44
27.0	1000.00	31.0	1148-15
.1	1003.70	-1	1151.85
.2	1007.41	.2	1155.56
.3	1011.11	-3	1159.26
.4	1014.81	.4	1162.96
.5	1018.52	-5	1166 6
.6	1022.22	.6	1170.37
.7	1025.93	.7	1174.07
.8	1029.63	.8	1177.78
.9	1033.33	.9	1181.48

Table 3.—Contents of Prisms 10 ft. wide and 100 ft. long.

Depths.	Contents.	Depths.	Contents.
32.0	1185.19	36.0.	1333.33
.1	1188.89	.1	1337.04
.2	1192.59	.2	1340.74
.3	1196.30	.3	1344.44
-4	1200.00	.4	1348.15
.5	1203.70	.5	1351.85
.6	1207.41	.6	1355.56
.7	1211.11	.7	1359.26
.8	1214.81	.8	1362.96
.9	1218.52	.9	1366.67
33.0	1222.22	37.0	1370.37
.1	1225.93	.1	1374.07
.2	1229.63	.2	1377.78
.3	1233.33	.3	1381.48
.4	1237.04	.4	1385.19
.5	1240.74	.5	1388.89
.6	1244.44	.6	1392.59
.7	1248.15	.7	1396.30
.8	1251.85	.8	. 1400.00
.9	1255.56	.9	1403.70
34.0	1259.26	38.0	1407.41
.1	1262.96	.1	1411.11
.2	1266.67	.2	1414.81
.3	1270.37	.3	1418.52
.4	1274.07	.4	1422.22
.5	1277.78	.5	1425.93
.6	1281.48	.6	1429.63
.7	1285.19	.7	1433.33
.8	1288.89	.8	1437.04
.9	1292.59	.9	1440.74
35.0	1296.30	39.0	1444.44
.1	1300.00	.1	1448.15
.2	1303.70	.2	1451.85
.3	1307.41	.3	1455.56
.4	1311.11	.4	1459.26
.5	1314.81	5	1462.96
.6	1318.52	.6	1466.67
.7	1322.22	.7	1470.37
.8	1325.93	.8	1474.07
.9	1329.63	.9	1477.78

Table 3.—Contents of Prisms 10 ft. wide and 100 ft. long.

Depths.	Contents.	Depths.	Contents.
40.0	1481.48	44.0	1629.63
.1	1485.19	.1	1633.33
.2	1488.89	.2	1637.04
.3	1492.59	.3	1640.74
.4	1496.30	.4	<b>1644</b> .44
.5	1500.00	.5	1648.15
.6	1503.70	.6	1651.85
.7	1507.41	.7	1655.56
.8	1511.11	.8	1659.26
.9	1514.81	.9	1662.96
41.0	1518.52	45.0	1666.67
.1	1522.22	.1	1670.37
.2	1525.93	.2	1674.07
.3	1529.63	.3	1677.78
.4	1533.33	.4	1681.48
.5	1537.04	.5	1685.19
.6	1540.74	.6	1688.89
.7	1544.44	.7	1692.59
.8 .	1548.15	.8	1696.30
.9	1551.85	.9	1700.00
42.0	1555.56	46.0	1703.70
.1	1559.26	.1	1703.70
.2	1562.96	.2	1711.11
.3	1566.67	.3	1714.81
.4	1570.37	.4	1718.52
.5	1574.07	.5	1722.22
.6	1577.78	.6	1725.93
.7	1581.48	.7	1729.63
.8	1585.19	.8	1733.33
.9	1588.89	.9	1737.04
43 0	1592.59	47.0	1740.74
.1	1596.30	.1	1740.74
.2	1600.00	.2	1744.44
.3	1603.70	.3	1740.15
. <b>3</b> . <b>4</b>	1607.41	.4	1751.65 1 <b>755</b> .56
.5	1611.11	.5	1759.26
.6 .6	1614.81	.6	1759.20 1762.96
.7	1618.52	.7	1762.90
.8	1618.52 1622.22	.8	1770.37
.8	1622.22 1625.93	.8	1770.37 1 <b>774</b> .07

Table 3.—Contents of Prisms 10 ft. wide and 100 ft. long.

Depths.	Contents.	Depths.	Contents.
48.0	1777.78	52.0	1925.93
.1	1781.48	.1	1929.63
.2	1785.19	.2	1933.33
.3	1788.89	.3	1937.04
.4	1792.59	.4	1940.74
.5	1796.30	.5	1944.44
.6	1800.00	.6	1948.15
.7	1803.70	.7	1951.85
.8	1807.41	.8	1955.56
.9	1811.11	.9	1959.26
49.0	1814.81	53.0	1962.96
.1	1818.52	.1	1966.67
.2	1822,22	.2	1970 37
.3	1825.93	.3	1974.07
.4	1829.63	.4	1977.78
.5	1833.33	.5	1981.48
.6	1837.04	.6	1985.19
.7	1840.74	.7	1988.89
.8	1844.44	.8	1992.59
.9	1848.15	.9	1996.30
50.0	1851.85	54.0	2000.00
.1	1855.56	.1	2003.70
.2	1859.26	.2	2007.41
.3	1862.96	.3	2011.11
.4	1866.67	.4	2014.81
.5	1870.37	.5	2018.52
.6	1874.07	.6	2022.22
.7	1877.78	.7	2025.93
.6	1881.48	.8	2029.63
.9	1885.19	.9	2033.33
51.0	1888.89	55.0	2037.04
.1	1892.59	.1	2040.74
.2	1896.30	.2	2044.44
.3	1900.00	.3	2048.15
.4	1903.70	.4	2051.85
.5	1907.41	.5	2055.56
.6	1911.11	.6	2059.26
.7	1914.81	.7	2062.96
.8	1918.52	.8	2066.67
.9	1922.22	.9	2070.37

Table 3.—Contents of Prisms 10 ft. wide and 100 ft. long.

Depths.	Contents.	Depths.	Contents.
56.0	2074.07	58.0	2148.15
.1	2077.78	.1	2151.85
.2	2081.48	.2	2155.56
.3	2085.19	.3	2159.26
<b>.4</b> :	2088.89	.4	2162.96
.5	2092.59	.5	2166.67
.6	2096.30	.6	2170.37
.7	2100.00	.7	2174.07
.8	2103.70	.8	2177.78
.9	2107.41	.9	2181.48
<b>57.0</b>	2111.11	59.0	2185.19
.1	2114.81	.1	2188.89
.2	2118.52	.2	2192.59
.3	2122.22	.3	2196.30
.4	2125.93	.4	2200.00
.5	2129.63	.5	2203.70
.6	2133.33	.6	2207.41
.7	2137.04	.7	2211.11
.8	2140.74	.8	2214.81
.9	2144.44	.9	2218.52

SOLID CONTENTS.

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

Length	Depth.					
II ing in	0.1	0.2	0.3	0.4	0.5	Length.
10	.37	.74	1.11	1.48	1.85	10
20	.74	1.48	2.22	2.96	3.70	20
30	1.11	2.22	3.33	4.44	5.55	30
40	1.48	2.96	4.44	5.92	7.40	40
50	1.85	3.70	5.55	7.40	9.25	50
60	<b>2.22</b>	4.44	6.66	8.88	11.10	60
70	2.59	5.18	7.77	10.36	12.95	70
80	2.96	5.92	8.88	11.84	14.80	80
90	3.33	6.66	9.99	13.32	16.65	90
100	3.70	7.40	11.10	14.80	18.50	100
Length	0.6	0.7	0.8	0.9	1.0	Length.
10	2.22	2.59	2.96	3.33	3.70	10
20	4.44	5.18	5.92	6.66	7.40	20
30	6.66	7.77	8.88	9.99	11.10	30
40	8.88	10.36	11.84	13.32	14.80	40 -
50	11.10	12.95	14.80	16.65	18.50	50
60	13.32	15.54	17.76	19.98	22.20	60
70	15.54	18.13	20.72	23.31	25.90	70
80	17.76	20.72	23.68	26.64	29.60	80
90	19.98	23.31	26.64	29.97	33.30	90
100	22.20	25.90	29.60	33.30	37.00	100
Length	1.1	1.2	1.3	1.4	1.5	Length.
10	4.07	4.44	4.81	5.19	5.56	10
20	8.14	8.88	9.62	10.38	11.12	20
30	12.21	13.32	14.43	15.57	16.68	30
40	16.28	17.76	19.24	20.76	22.24	40
50	20.35	22.20	24.05	25.95	27.80	50
60	24.42	26.64	28.86	31.14	33.36	60
70	28.49	31.08	33.67	36.33	38.92	70
80	32.56	35.52	38.48	41.52	44.48	80
90	36.63	39.96	43.29	46.71	50.04	90
100	40.70	44.40	48.10	51.90	55.60	100
•	7					

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

Length	Depth.						
	1.6	1.7	1.8	1.9	2.0	Length	
10	5.93	6.30	6.67	7.04	7.41	10	
20	11.86	12.60	13.34	14.08	14.82	20	
30	17.79	18.90	20.01	21.12	22.23	30	
40	23.72	25.20	26.68	28.16	29.64	40	
50	29.65	31.50	33.35	35.20	37.05	50	
60	35.58	37.80	40.02	42.24	44.46	60	
70	41.51	44.10	46.69	49.28	51.87	70	
80	47.44	50.40	53.36	56.32	59.28	80	
90	53.37	56.70	60.03	63.36	66.69	90	
100	<b>59.30</b>	63.00	66.70	70.40	74.10	100	
Length	2.1	2.2	2.3	2.4	2.5	Length.	
10	7.78	8.15	8.52	8.89	9.26	10	
20	15.56	16.30	17.04	17.78	18.52	20	
30	23.34	24.45	25.56	26.67	27.78	30	
40	31.12	32.60	34.08	35.56	37.04	40	
50	38.90	40.75	42.60	44.45	46.30	50	
60	46.68	48.90	51.12	53.34	55.56	60	
70	54.46	57.05	59.64	62.23	64.82	70	
80	62.24	65.20	68.16	71.12	74.08	80	
90	70.02	73.35	76.68	80.01	83.34	90	
100	77.80	81.50	.85.20	88.90	92.60	100	
Length	2.6	2.7	2.8	2.9	3.0	Length.	
10	9.63	10.00	10.37	10.74	11.11	10	
20	19.26	20.00	20.74	21.48	22.22	20	
30	28.89	30.00	31.11	32.22	33.33	30	
40	38.52	40.00	41.48	42.96	44.44	40	
50	48.15	50.00	51.85	53.70	55.55	50	
60	57.78	60.00	62.22	64.44	66.66	60	
70	67.41	70.00	72.59	75.18	77.77	70	
80	77.04	80.00	82.96	85.92	88.88	80	
90	86.67	90.00	93.33	96.66	99.99	90	
100	96.30	100.00	103.70	107.40	111.10	100	

SOLID CONTENTS.

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

Length.		Depth.				
Len	3.1	3.2	3.3	3.4	3.5	Length.
10	11.48	11.85	12.22	12.59	12.96	10
20	22.96	23.70	24.44	25.18	25.92	20
30	34.44	35.55	36.66	37.77	38.88	30
<b>4</b> 0	45.92	47.40	48.88	50.36	51.84	40
<b>5</b> 0	57.40	59.25	61.10	62.95	64.80	50
60	68.88	71.10	73.32	75.54	77.76	60
70	80.36	82.95	85.54	88.13	90.72	70
80	91.84	94.80	97.76	100.72	103.68	80
90	103.32	106.65	109.98	113.31	116.64	90
100	114.80	118.50	122.20	125.90	129.60	100
L.	3.6 `	3.7	3.8	3.9	4.0	<b>L</b> .
10	13.33	13.70	14.07	14.44	14.82	10
20	26.66	27.40	28.14	28.88	29.64	20
30	39.99	41.10	42.21	43.32	44.46	30
40	53.32	54.80	56.28	57.76	59.28	40
50	66.65	68.50	70.35	72.20	74.10	50
60	79.98	82.20	84.42	86.64	88.92	60
70	93.31	95.90	98.49	101.08	103.74	70
80	106.64	109.60	112.56	115.52	118.56	80
90	119.97	123.30	126.63	129.96	133.38	90
100	133.30	137.00	140.70	144.40	148.20	100
<i>L</i> .	4.1	4.2	4.3	4.4	4.5	L.
10	15.19	15.56	15.93	16.30	16.67	10
20	30.38	31.12	31.86	32.60	33.34	20
80	45.57	46.68	47.79	48.90	50.01	30
40	60.76	62.24	63.72	65.20	66.68	40
50	75.95	77.80	79.65	81.50	83.35	50
60	91.14	93.36	95.58	97.80	100.02	60
70	106.33	108.92	111.51	114.10	116.69	70
80	121.52	124.48	127.44	130.40	133.36	80
90	136.71	140.04	1 <b>43.37</b>	146.70	150.03	90
100	151.90	155.60	159.30	163.00	166.70	100

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

th.		-	Depth.			li.
Length.	4.6	4.7	4.8	4.9	5.0	Length.
10	17.04	17.41	17.78	18.15	18.52	10
20	34.08	34.82	35.56	36.30	37.04	20
30	51.12	52.23	53.34	54.45	55.56	30
40	68.16	69.64	71.12	72.60	74.08	40
<b>5</b> 0	85.20	87.05	88.90	90.75	92.60	50
60	102.24	104.46	106.68	108.90	111.12	60
70	119.28	121.87	124.46	127.05	129.64	70
80	136.32	139.28	142.24	145.20	148.16	80
90	153.36	156. <b>6</b> 9	160.02	163.35	166.68	90
100	170.40	174.10	177.80	181.50	185.20	100
L.	5.1	5.2	5.3	5.4	5.5	L.
10	18.89	19.26	19.63	20.00	20.37	10
20	37.78	38.52	39.26	40.00	40.74	20
<b>3</b> 0	56.67	57.78	58.89	60.00	61.11	30
40	75.56	77.04	78.52	80.00	81.48	40
<b>5</b> 0	94.45	96.30	98.15	100.00	101.85	50
60	113.34	115.56	117.78	120.00	122.22	60
70	132.23	134.82	137.41	140.00	142.59	70
80	151.12	154.08	157.04	160.00	162.96	80
90	170.01	173.34	176.67	180.00	183.33	90
100	188.90	192.60	196.30	200.00	203.70	100
$\overline{L}$ .	5.6	5.7	5.8	5.9	6.0	L.
10	20.74	21.11	21.48	21.85	22.22	10
20	41.48	42.22	42.96	43.70	44.44	20
<b>3</b> 0	62.22	63.33	64.44	65.55	66.66	30
<b>4</b> 0	82.96	84.44	85.92	87.40	88.88	40
<b>50</b>	103.70	105.55	107.40	109.25	111.10	50
60	124.44	126.66	128.88	131.10	133.32	60
70	145.18	147.77	150.36	152.95	155.54	70
80	165.92	168.88	171.84	174.80	177.76	80
90	186.66	189.99	193.32	196.65	199.98	90
100	207.40	211.10	214.80	218.50	222.20	100

SOLID CONTENTS.

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

gth.			${\it Depth}$ .	•		gth.
Length.	6.1	6.2	6.3	6.4	6.5	Length.
10	22.59	22.96	23.33	23.70	24.07	10
20	45.18	45.92	46.66	47.40	48.14	20
30	67.77	68.88	69.99	71.10	72.21	30
40	90.36	91.84	93.32	94.80	96.28	40
50	112.95	114.80	116 65	118.50	120.35	50
60	135.54	137.76	139.98	142.20	144.42	60
70	158.13	160.72	163.31	165.90	168.49`	70
80	180.72	183.68	186.64	189.60	192.56	80
90	203.31	206.64	209.97	213.30	216.63	90
100	225.90	229.60	233.30	237.00	240.70	100
L.	6.6	6.7	6.8	6.9	7.0	L.
10	24.44	24.82	25.19	25,56	25.93	10
20	48.88	49.64	50.38	51.12	51.86	20
30	73.32	74.46	75.57	76.68	77.79	30
40	97.76	99.28	100.76	102.24	103.72	40
<b>50</b>	122.20	124.10	125.95	127.80	129.65	50
60	146.64	148.92	151.14	153.36	155.58	60
70	171.08	173.74	176.33	178.92	181.51	70
80	195.52	198.56	201.52	204:48	207.44	80
90	219.96	223.38	226.71	230.04	233.37	90
100	244.40	248.20	251.90	255.60	259.30	100
L.	7.1	7.2	7.3	7.4	7.5	L.
10	26.30	26.67	27.04	27.41	27.78	10
20	52.60	53.34	54.08	54.82	55.56	20
30	78.90	80.01	81.12	82.23	83.34	30
40	105.20	106.68	108.16	109.64	111.12	40
50	131.50	133.35	135.20	137.05	138.90	50
60	157.80	160.02	162.24	164.46	166.68	60
70	184.10	186.69	189.28	191.87	194.46	70
80	210.40	213.36	216.32	219.28	222.24	80
90	236.70	240.03	243.36	246.69	250.02	90
100	263.00	266.70	270.40	274.10	277.80	100

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

				J		
gth.			Depth.			gth.
Length.	7.6	7.7	7.8	7.9	8.0	Length.
10	28.15	28.52	28.89	29.26	29.63	10
20	56.30	57.04	57.78	58.52	59.26	20
<b>3</b> 0	84.45	85.56	86.67	87.78	88.89	30
40	112.60	114.08	115.56	117.04	118.52	40
<b>5</b> 0	140.75	142.60	144.45	146.30	148.15	50
<b>6</b> 0	168.90	171.12	173.34	175.56	177.78	60
70	197.05	199.64	202.23	204.82	207.41	70
80	225.20	228.16	231.12	234.08	237.04	80
90	253.35	256.68	260.01	263.34	266.67	90
100	281.50	285.20	288.90	292.60	296.30	100
<i>L</i> .	8.1	8.2	8.3	8.4	8.5	<b>L</b> .
10	30.00	30.37	30.74	81.11	31.48	10
20	60.00	60.74	61.48	62.22	62.96	20
30	90.00	91.11	92.22	93.33	94.44	30
40	120.00	121.48	122,96	124.44	125.92	40
<b>5</b> 0	150.00	151.85	153.70	155.55	157.40	50
<b>6</b> 0	180.00	182.22	184.44	186.66	188.88	60
70	210.00	212.59	215.18	217.77	220.36	70
80	240.00	242.96	245.92	248.88	251.84	80
90	270.00	273.33	276.66	279.99	283.32	90
100	300.00	303.70	807.40	311.10	314.80	100
L.	8.6	8.7	8.8	8.9	9.0	L.
10	31.85	32.22	32.59	32.96	33.33	10
20	63.70	64.44	65.18	65.92	66.66	20
30	95.55	96.66	97.77	98.88	99.99	30
40	127.40	128.88	130.36	131.84	133.32	40
<b>5</b> 0	159.25	161.10	162.95	164.80	166.65	50
60	191.10	193.32	195.54	197.76	199.98	60
70	222.95	225.54	228.13	230.72	233.31	70
80	254.80	257.76	260.72	263.68	<b>266.64</b>	80
90	286.65	289.98	293.31	296.64	299.97	90
100	318.50	322.20	325.90	329.60	333.30	100

SOLID CONTENTS.

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

gth.			Depth.			gth.
Length.	9.1	9.2	9.3	9.4	9.5	Length
10	33.70	34.07	34.44	34.82	35.19	10
20	67.40	68.14	68.88	69.64	70.38	20
30	101.10	102.21	103.32	104.46	105.57	30
40	134.80	136.28	137.76	139.28	140.76	40
50	168.50	170.35	172.20	174,10	175.95	50
60	202.20	204.42	206.64	208.92	211.14	60
70	235.90	238.49	241.08	243.74	246.33	70
80	269.60	272 56	275.52	278.56	281.52	80
90	303.30	306.63	309.96	313.38	316.71	90
100	337.00	340.70	344.40	348.20	351.90	100
<b>L</b> .	9.6	9.7	9.8	9.9	10.0	L.
10	35.56	<b>3</b> 5 93	36.30	36.67	37.04	10
20	71.12	71.86	72.60	73.34	74.08	20
30	106.68	107.79	108.90	110.01	111.12	30
40	142.24	143.72	145.20	146.68	748.16	40
50	177.80	179.65	181.50	183.35	185.20	50
<b>6</b> 0	213.36	215.58	217.80	220.02	222.24	60
70	248.92	251.51	254.10	256.69	259.28	70
80	284.48	287.44	290.40	293.36	296.32	80
90	320.04	323.37	326.70	330.03	333.36	90
100	355.60	359.30	363.00	366.70	370.40	100
L.	10.1	10.2	10.3	10.4	10.5	L.
10	37.41	37.78	38.15	38.52	38.89	10
20	74.82	75.56	76.30	77.04	77.78	20
30	112.23	113.34	114.45	115.56	116.67	30
40	149.64	151.12	152.60	154.08	155.56	40
<b>5</b> 0	187.05	188.90	190.75	192.60	194.45	50
60	224.46	226.68	228.90	231.12	233.34	60
70	261.87	264.46	267.05	269.64	272.23	70
80	299.28	302.24	305.20	308.16	311.12	80
90	336.69	340.02	343.35	346.68	350.01	90
100	374.10	377.80	381.50	385.20	388.90	100

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

gth.			Depth.			gth.
Length.	10.6	10.7	10.8	10.9	11.0	Length.
10	39.26	39.63	40.00	40.37	40.74	10
20	78.52	79.26	80.00	80.74	81.48	20
<b>30</b>	117.78	118.89	120.00	121.11	122.22	30
<b>4</b> 0	157.04	158.52	160.00	161.48	162.96	40
50	196.30	198.15	200.00	201.85	203.70	50
<b>6</b> 0	235.56	237.78	240.00	242.22	244.44	60
70	274.82	277.41	280.00	282.59	285.18	70
80	314.08	317.04	320.00	322.96	325.92	80
90	<b>3</b> 53.34	356.67	360.00	363.33	366.66	90
100	392.60	396.30	400.00	403.70	407.40	100
L.	11.1	11.2	11.3	11.4	11.5	L.
10	41.11	41.48	41.85	42.22	42.59	10
20	82.22	82.96	83.70	84.44	85.18	20
30	123.33	124.44	125.55	126.66	127.77	30
40	164.44	165.92	167.40	168.88	170.36	40
<b>50</b>	205.55	207.40	209.25	211.10	212.95	50
60	246.66	248.88	251.10	253.32	255.54	60
70	287.77	290.36	292.95	295.54	298.13	70
80	328.88	331.84	334.80	337.76	340.72	80
90	369.99	373.32	<b>376</b> .65	379.98	383.31	90
100	411.10	414.80	418.50	422.20	425.90	100
L.	11.6	11.7	11.8	11.9	12.0	<i>L</i> .
10	42.96	43.33	43.70	44.07	44.44	10
<b>20</b>	85.92	86.66	87.40	88.14	88.88	20
30	128.88	129.99	131.10	132.21	133.32	30
40	171.84	173.32	174.80	176.28	177.76	40
<b>50</b>	214.80	216.65	218.50	220.35	222.20	50
60	257.76	259.98	262.20	264.42	266.64	60
70	300.72	303.31	305.90	308.49	311.08	70
80	343.68	346.64	349.60	352.56	<b>355.52</b>	80
90	386.64	389.97	393.30	396.63	<b>399.96</b>	90
100	429.60	433.30	437.00	440.70	444.40	100

SOLID CONTENTS.

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

gth.			Depth.			gth.
Length.	12.1	12.2	12.3	12.4	12.5	Length.
10	44.81	45.19	45.56	45.93	46.30	10
20	89.62	90.38	91.12	91.86	92.60	20
30	134.43	135.57	136.68	137.79	138.90	30
40	179.24	180.76	182.24	183.72	185.20	40
50	224.05	225.95	227.80	229.65	231.50	50
60	268.86	271.14	273.36	275.58	277.80	60
70	313.67	316.33	318.92	321.51	324.10	70
80	358.48	361.52	364.48	367.44	370.40	80
90	403.29	406.71	410.04	413.37	416.70	90
100	448.10	451.90	455.60	459.30	463.00	100
L.	12.6	12.7	12.8	12.9	13.0	L.
10.	46.67	47.04	47.41	47.78	48.15	10
20	93.34	94.08	94.82	95.56	96.30	20
30	140.01	141.12	142.23	143.34	144.45	30
40	186.68	188.16	189.64	191.12	192.60	40
50	233.35	235.20	237.05	238.90	240.75	50
60	280.02	282.24	284.46	286.68	288.90	60
70	326.69	329.28	331.87	334.46	337.05	70
80	373.36	376.32	379.28	382.24	385.20	80
90	420.03	423.36	426.69	430.02	433.35	90
100	466.70	470.40	474.10	477.80	481.50	100
<i>L</i> .	13.1	13.2	13.3	13.4	13.5	L.
10	48.52	48.89	49.26	49.63	50.00	10
20	97.04	97.78	98.52	99.26	100.00	20
30	145.56	146.67	147.78	148.89	150.00	30
40	194.08	195.56	197.04	198.52	200.00	40
50	242.60	244.45	246.30	248.15	250.00	50
60	291.12	293.34	295.56	297.78	300.00	60
70	339.64	342.23	344.82	347.41	<b>35</b> 0. <b>0</b> 0	70
80	388.16	391.12	394.08	397.04	400.00	80
90	436.68	440.01	443.34	446.67	450.00	90
100	485.20	488.90	492.60	496.30	500.00	100
	8					

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

Length.			Depth.			gth.
Len	13.6	13.7	13.8	13.9	14.0	200 200 300 400 500 600 1000 L.
10	50.37	50.74	51.11	51.48	51.85	10
20	100.74	101.48	102.22	102.96	103.70	20
<b>3</b> 0	151.11	152.22	153.33	154.44	155.55	30
40	201.48	202.96	204.44	205.92	207.40	40
<b>5</b> 0	251.85	253.70	255.55	257.40	259.25	50
<b>6</b> 0	302.22	304.44	306.66	308.88	311.10	60
70	<b>352.59</b>	355.18	357.77	360.36	362.95	70
80	402.96	405.92	408.88	411.84	414.80	80
90	453.33	456.66	459.99	463.32	466.65	90
100	503.70	507.40	511.10	514.80	518.50	100
L.	14.1	14.2	14.3	14.4	14.5	L.
10	52.22	52.59	52.96	53.33	53.70	10
20	104.44	105.18	105.92	106.66	107.40	20
30	156.66	157.77	158.88	159.99	161.10	30
40	208.88	210.36	211.84	213.32	214.80	40
50	261.10	262.95	264.80	266.65	268.50	50
60	313.32	315.54	317.76	319.98	322.29	60
70	365.54	368.13	370.72	373.31	375.90	70
80	417.76	420.72	423.68	426.64	429.60	80
90	469.98	473.31	476.64	479.97	483.30	90
100	522.20	525.90	529.60	533.30	537.00	100
<b>L</b> .	14.6	14.7	14.8	14.9	15.0	L.
10	54.07	54.44	54.82	55.19	55.56	10
20	108.14	108.88	109.64	110.38	111.12	20
30	162.21	163.32	164.46	165.57	166.68	30
40	216.28	217.76	219.28	220.76	222.24	40
50	270.35	272.20	274.10	275:95	277.80	50
60	324.42	326.64	328.92	331.14	333.36	60
70	378.49	381.08	383.74	386.33	388.92	70
80	432.56	435.52	438.56	441.52	444.48	80
90	486.63	489.96	493.38	496.71	500.04	90
100	540.70	544.40	548.20	551.90	555.60	100

SOLID CONTENTS.

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

gth.			Depth.			gth.
Length.	15.1	15.2	15.3	15.4	15.5	Length.
10	55.93	56.30	56.67	57.04	57.41	10
20	111.86	112.60	113.34	114.08	114.82	20
30	167.79	168.90	170.01	171.12	172.23	30
40	223.72	225.20	226.68	228.16	229.64	40
<b>50</b>	279.65	281.50	283.35	285.20	287.05	50
<b>6</b> 0	335.58	337.80	340.02	342.24	344.46	60
70	<b>3</b> 91.51	394.10	<b>396.69</b>	399.28	401.87	70
80	447.44	450.40	453.36	456.32	459.28	80
90	503.37	506.70	510.03	513.36	516.69	90
100	559.30	563.00	566.70	570.40	574.10	100
L.	15.6	15.7	15.8	15.9	16.0	L.
10	57.78	58.15	58.52	58.89	59.26	10
20	115.56	116.30	117.04	117.78	118.52	20
30	173.34	174.45	175.56	176.67	177.78	30
40	231.12	232.60	234.08	235.56	237.04	40
50	288.90	290.75	292.60	294.45	296.30	50
60	346.68	348.90	351.12	353.34	355.56	60
70	404.46	407.05	409.64	412.23	414.82	70
80	462.24	<b>46</b> 5.20	468.16	471.12	474.08	80
90	520.02	<b>523.35</b>	<b>526.68</b>	530.01	533.34	90
100	577.80	581.50	585.20	588.90	592.60	100
L.	16.1	16.2	16.3	16.4	16.5	L.
10	59.63	60.00	60.37	60.74	61.11	10
20	119.26	120.00	120.74	121.48	122.22	20
80	178.89	180.00	181.11	182.22	183.33	30
40	238.52	240.00	241.48	242.96	244.44	40
<b>50</b>	298.15	300.00	301.85	303.70	305.55	50
`60	357.78	360.00	362.22	364.44	<b>366.66</b>	60
70	417.41	420.00	422.59	425.18	427.77	70
80	477.04	480.00	482.96	485.92	488.88	80
90	536.67	540.00	543.33	546.66	549.99	90
100	596.80	600.00	603.70	607.40	611.10	100

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

gth.			Depth.			gth.
Length.	16.6	16.7	16.8	16.9	17.0	Length.
10	61.48	61.85	62.22	62.59	62.96	10
20	122.96	123.70	124.44	125.18	125.92	20
30	184.44	185.55	186.66	187.77	188.88	30
40	245.92	247.40	248.88	250.36	251.84	40
<b>50</b>	307.40	309.25	311.10	312.95	314.80	50
<b>,6</b> 0	368.88	371.10	373.32	375.54	377.76	60
70	430.36	<b>43</b> 2.95	435.54	438.13	440.72	70
80	491.84	494.80	497.76	500.72	503.68	80
90	553.32	556.65	559.98	563.31	566.64	90
100	614.80	618.50	622.20	625.90	629.60	100
L.	17.1	17.2	17.3	17.4	17.5	L.
10	63.33	63.70	64.07	64.44	64.81	10
20	126.66	127.40	128.14	128.88	129.62	20
30	189.99	191.10	192.21	193.32	194.43	30
40	253.32	254.80	256.28	257.76	259.24	40
50	316.65	318.50	320.35	322.20	324.05	50
60	379.98	382.20	384.42	386.64	388.86	60
70	443.31	445.90	448.49	451.08	453.67	70
80	506.64	<b>509.60</b>	512.56	515.52	518.48	80
90	569.97	573.30	576.63	579.96	583.29	90
100	633.30	637.00	640.70	644.40	648.10	100
L.	17.6	17.7	17.8	17.9	18.0	L.
10	65.19	65.56	65.93	66.30	66.67	10
20	130.38	131.12	131.86	132.60	133.34	20
30	195.57	196.68	197.79	198.90	200.01	30
40	260.76	262.24	263.72	265.20	266.68	40
<b>50</b>	325.95	327.80	329.65	331.50	333. <b>3</b> 5	50
60	391.14	393.36	395.58	397.80	400.02	60
70	456.33	458.92	461.51	464.10	466.69	70
80	521.52	<b>524.48</b>	527.44	530.40	533.36	80
90	586.71	590.04	593,37	596.70	600.03	90
100	651.90	655.60	659.30	663.00	666.70	100

SOLID CONTENTS.

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

gth.			Depth.			gth.
Length.	18.1	18.2	18.3	18.4	18.5	Length.
10	67.04	67.41	67.78	68.15	68.52	10
20	134.08	134.82	135.56	136.30	137.04	20
30	201.12	202.23	203.34	204.45	205.56	30
<b>4</b> 0	268.16	269.64	271.12	272.60	274.08	40
<b>50</b>	335.20	337.05	338.90	340.75	342.60	50
60	402.24	404.46	406.68	408.90	411.12	60
70	469.28	471.87	474.46	477.05	479.64	70
80	536.32	539.28	542.24	545.20	548.16	80
90	603.36	606.69	610.02	613.35	616.68	90
100	670.40	674.10	677.80	681.50	685.20	100
<b>L</b> .	18.6	18.7	18.8	18.9	19.0	L.
10	68.89	69.26	69.63	70.00	70.37	10
20	137.78	138.52	139.26	140.00	140.74	20
30	206.67	207.78	208.89	210.00	211.11	30
40	275.56	277.04	278.52	- 280.00	281.48	40
50	344.45	346.30	348.15	350.00	351.85	50
60	413.34	415.56	417.78	420.00	422.22	60
70	482.23	484.82	487.41	490.00	492.59	70
80	<b>5</b> 51.12	554.08	557.04	<b>56</b> 0.00	562.96	80
90	620.01	623.34	626.67	630.00	633.33	90
100	688.90	692.60	696.30	700.00	703.70	100
L.	19.1	19.2	19.3	19.4	19.5	L.
10	70.74	71.11	71.48	71.85	72.22	10
20	141.48	142.22	142.96	143.70	144.44	20
30	212.22	213.33	214.44	215.55	216.66	30
40	282.96	284.44	285.92	287.40	288.88	40
50	353.70	355.55	357.40	359.25	361.10	50
60	424.44	426.66	428.88	431.10	433.32	60
70	495.18	497.77	500.36	502.95	505.54	70
80	565.92	568.88	571.84	574.80	577.76	80
90	636.66	639.99	643.32	646.65	649.98	90
100	707.40	711.10	714.80	718.50	722.20	100

Supplement to table 3.—Prisms 10 feet wide.—Solid contents.

gth.	_	-	Depth.			10 20 30 40 40 40 40 40 40 40 40 40 40 40 40 40
Longth.	19.6	19.7	19.8	19.9	20.0	Len
10	72.59	72.96	73.33	73.70	74.07	10
20	145.18	145.92	146.66	147.40	148.14	20
30	217.77	218.88	219.99	221.10	222.21	30
40	290.36	291.84	293.32	294.80	296.28	40
50	362.95	364.80	366 65	368.50	370.35	50
60	435.54	437.76	439.98	442.20	444.42	60
70	508.13	510.72	513.31	515.90	518.49	70
80	580.72	583.68	586.64	589.60	592.56	80
90	653.31	656.64	659.97	663.30	666.63	90
100	725.90	729.60	733.30	737.00	740.70	100

Table 4.—Contents of Slopes, for a slope of  $2\frac{1}{4}$  to 1, and for a length of 100 feet.

Depths.	Contents.	D.	Depths.	Contents.	Ď.
			4.0	148.15	7.50
0.1	.09	.28	.1	155.65	7.69
.2	.37	.46	.2	163.33	7.87
.3	.83	.65	.3	171.20	8.06
.4	1.48	.83	.4	179.26	8.24
.5	2.31	1.02	.5	187.50	8.43
.6	3.33	1.20	.6	195.93	8.61
.7	4.54	1.39	.7	204.54	8.80
.8	5.93	1.57	.8	213.33	8.98
.9	7.50	1.76	.9	222.31	9.17
1.0	9.26	1.94	5.0	231.48	9.35
.1	11.20	2.13	.1	240.83	9.54
.2	13.33	2.31	.2	250.37	9.72
.3	15.65	2.50	.3	260.09	9.91
.4	18.15	2.69	.4	270.00	10.09
.5	20.83	2.87	.5	280.09	10.28
.6	23.70	3.06	.6	290.37	10.46
.7	26.76	3.24	.7	300.83	10.65
.8	30.00	3.43	.8	311.48	10.83
.9	33.43	3.61	.9	322.31	11.02
2.0	37.04	3.80	6.0	333.33	11.20
.1	40.83	3.98	.1	344.54	11.39
.2	44.81	4.17	.2	<b>355.93</b>	11.57
.3	48.98	<b>4.35</b>	.3	367.50	11.76
.4	53.33	4.54	.4	379.26	11.94
.5	57.87	4.72	-5	<b>391.20</b>	12.13
.6	62.59	4.91	-6	403.33	12.31
.7	67.50	5.09	.7	415.65	12.50
.8	72.59	5.28	-8	428.15	12.69
.9	77.87	5.46	.9	440.83	12.87
3.0	83.33	5.65	7.0	453.70	13.06
.1	88.98	5.83	-1	466.76	13.24
.2	94.81	6.02	.2	480.00	13.43
.3	100.83	6.20	.3	493.43	13.61
.4	107.04	6.39	-4	507.04	13.80
.5	113.43	6.57	-5	<b>520.83</b>	13.98
.6	120.00	6.76	-6	534.81	14.17
.7	126.76	6.94	.7	<b>548.98</b>	14.35
.8	133.70	7.13	-8	<b>563.33</b>	14.54
Ω.	140.83	7.31	.9	577.87	14.72

Table 4.—Contents of Slopes, for a slope of 2½ to 1, and for a length of 100 feet.

Depths.	Contents.	<b>D</b> .	Depths.	Contents.	D.
8.0	592.59	14.91	12.0	1333.33	22.31
.1	607.50	15.09	.1	1355.65	22.50
.2	622.59	15.28	.2	1378.15	22.69
.3	637.87	15.46	.3	1400.83	22.87
.4	653.33	15.65	.4	1423.70	23.06
.5	668.98	15.83	.5	1446.76	23.23
.6	684.81	16.02	.6	1470.00	23.43
.7	700.83	16.20	.7	1493.43	23.61
.8	717.04	16.39	.8	1517.04	23.80
.9	733.43	16.57	.9	1540.83	23.98
9.0	750.00	16.76	13.0	1564.81	24.17
.1	766.76	16.94	.1	1588.98	24.35
.2	783.70	17.13	.2	1613.33	24.54
.3	800.83	17.31	.3	1637.87	24.72
.4	818.15	17.50	.4	1662.59	24.91
.5	835.65	17.69	.5	1687.50	25.09
.6	853.33	17.87	.6	1712.59	25.28
.7	871.20	18.06	.7	1737.87	25.46
.8	889.26	18.24	.8	1763.33	25.65
.9	907.50	18.43	.9	1788.98	25.83
10.0	925.93	18.61	14.0	1814.81	26.02
.1	944.54	18.80	.1	1840.83	26.20
.2	963.33	18.98	.2	1867.04	26.39
.3	982.31	19.17	.3	1893.43	26.57
.4	1001.48	19.35	.4	1920.00	26.76
.5	1020.83	19.54	.5	1946.76	26.94
.6	1040.37	19.72	.6	1973.70	27.13
.7	1060.09	19.91	.7	2000.83	27.31
.8	1080.00	20.09	.8	2028.15	27.50
.9	1100.09	20.28	.9	2055.65	27.69
11.0	1120.37	20.46	15.0	2083.33	27.87
.1	1140.83	20.65	.1	2111.20	28.06
.2	1161.48	20.83	.2	2139.26	28.24
.3	1182.31	21.02	.3	2167.50	28.43
.4	1203.33	21.20	.4	2195.93	28.61
.5	1224.54	21.39	.5	2224.54	28.80
.6	1245.93	21.57	.6		28.98
.7	1267.50	21.76	.7	2282.31	29.17
.8	1289.26	, 21.94	8	2311.48	29.35
.9	1311.20	22.13	Ω.	2340.83	29.54

Table 4.—Contents of Slopes, for a slope of 2½ to 1, and for a length of 100 feet.

Depths.	Contents.	D.	Depths.	Contents.	D.
16.0	2370.37	29.72	20.0	3703.70	37.13
.1	2400.09	29.91	.1	3740.83	37.31
.2	2430.00	30.09	.2	3778.15	37.50
.8	2460.09	30.28	.3	3815.65	37.69
.4	2490.37	30.46	.4	3853.33	37.87
.5	2520.83	30.65	.5	3891.20	38.06
.6	2551.48	30.83	.6	3929.26	38.24
.7	2582:31	31.02	.7	3967.50	38.43
.8	2613.33	31.20	.8	4005.93	38.61
.9	2644.54	31.39	.9	4044.54	38.80
17.0	2675.93	31.57	21.0	4083.33	38.98
.1	2707.50	31.76	.1	4122.31	39.17
.2	<b>2739.26</b>	31.94	.2	4161.48	39.35
.3	2771.20	32.13	.3	4200.83	39.54
.4	2803.33	32.31	.4	4240.37	39.72
.5	2835.65	32.50	.5	4280.09	39.91
.6	2868.15	32.69	.6	4320.00	40.09
.7	2900.83	32.87	.7	4360.09	40.28
.8	2933.70	33.06	.8	4400.37	40.46
.9	2966.76	33.24	.9	4440.83	40.65
18.0	3000.00	33.43	22.0	4481.48	40.83
.1	3033.43	33.61	.1	4522.31	41.02
.2	3067.04	33.80	.2	4563.33	41.20
.3	3100.83	33.98	.3	4604.54	41.39
.4	3134.81	34.17	.4	4645.93	41.57
.5	3168.98	34.35	.5	4687.50	41.76
.6	3203.33	34.54	.6	4729.26	41.94
.7	3237.87	34.72	.7	4771.20	42.13
.8	3272.59	34.91	.8	4813.33	<b>42.31</b>
.9	3307.50	35.09	.9	4855.65	42.50
19.0	<b>3342</b> .59	35.28	23.0	4898.15	42.69
.1	3377.87	35.46	.1	4940.83	42.87
.2	<b>34</b> 13.33	35.65	.2	4983.70	43.06
.3	3448.98	35.83	.3	5026.76	43.24
.4	<b>34</b> 84.81	36.02	.4	5070.00	43.43
.5	3520.83	36.20	.5	5113.43	43.61
.6	3557.04	36.39	.6	5157.04	43.80
.7	<b>3593.43</b>	36.57	.7	5200.83	43.98
.8	<b>3630.0</b> 0	36.76	.8	<b>5244</b> .81	44.17
.9	3666.76	36.94	.9	<b>5288.98</b>	44.35

Table 4.—Contents of Slopes, for a slope of  $2\frac{1}{4}$  to 1, and for a length of 100 feet.

Depths.	Contents.	<b>D</b> .	Depths.	Contents.	D.
24.0	5333.33	44.54	28.0	7259.26	51.94
.1	5377.87	44.72	.1	7311.20	52-13
.2	5422.59	44.91	.2	7363.33	52.31
.3	5467.50	45.09	.3	7415.65	<b>5</b> 2.50
.4	5512.59	45.28	.4	7468.15	<b>52.69</b>
.5	5557.87	45.46	.5	7520.83	52.87
.6	5603.33	45.65	.6	7573.70	53.06
.7	5648.98	45.83	.7	7626 76	53.24
.8	5694.81	46.02	.8	7680.00	53.43
.9	5740.83	46.20	.9	7733.43	53.61
25.0	5787.04	46.39	29.0	7787.04	53.80
.1	5833.43	46.57	.1	7840.83	<b>53</b> .98
.2	5880.00	46.76	.2	7894.81	54.17
.3	5926.76	46.94	.3	7948.98	54.35
.4	5973.70	47.13	.4	8003.33	54.54
.5	6020.83	47.31	.5	8057.87	54.72
.6	6068.15	47.50	.6	8112.59	54.91
.7	6115.65	47.69	.7	8167.50	55.09
.8	6163.33	47.87	.8	8222.59	55.28
.9	6211.20	48.06	.9	8277.87	55.46
<b>26</b> .0	6259.26	48.24	30.0	8333.33	55.65
.1	6307.50	48.43	.1	8388.98	<b>5</b> 5.83
.2	6355.93	48.61	.2	8444.81	56.02
.3	6404.54	48.80	.3	8500.83	56.20
.4	6453.33	48.98	.4	8557.04	56.39
.5	6502.31	49.17	.5	8613.43	56.57
.6	6551.48	49.35	.6	8670.00	56.76
.7	6600.83	49.54	.7	8726.76	56.94
.8	6650.37	49.72	.8	8783.70	57.13
.9	6700.09	49.91	.9	8840.83	57.31
27.0	6750.00	50.09	31.0	8898.15	57.50
.1	6800.09	50.28	.1	<b>8955.65</b>	57.69
.2	6850.37	50.46	.2	9013.33	57.87
.3	6900.83	50.65	.3	9071.20	58.06
.4	6951.48	50.83	.4	9129.26	58.24
.5	7002.31	51.02	.5	9187.50	58.43
.6	7053.33	51.20	.6	9245.93	58.61
.7	7104.54	51.39	.7	9304.54	58.80
8	7155.93	51.57	.8	9363.33	58.98
.9	7207.50	51.76	.9	9422.31	59.17

Table 4.—Contents of Slopes, for a slope of  $2\frac{1}{2}$  to 1, and for a length of 100 feet.

Depths.	Contents.	<b>D</b> .	Depths.	Contents.	D.
32.0	9481.48	59.35	36.9	12000.00	66.76
.1	9540.83	59.54	.1	12066.76	66.94
.2	9600.37	59.72	.2	12133.70	67.13
.3	9660.09	59.91	.3	12200.83	67.31
.4	9719.99	60.09	.4	12268.15	67.50
.5	9780.09	60.28	.5	12335.65	67.69
.6	9840.37	60.46	.6	12403.33	67.87
.7	9900.83	60.65	.7	12471.20	68.06
.8	9961.48	60.83	.8	12539.26	68.24
.9	10022.31	61.02	.9	12607.50	68.43
33.0	10083.33	61.20	37.0	12675.93	68.61
.1	10144.54	61.39	.1	12744.54	68.80
.2	10205.93	61.57	.2	12813.33	68.98
.3	10267.50	61.76	.3	12882.31	69.17
.4	10329.26	61.94	.4	12951.48	69.35
.5	10391.20	62.13	.5	13020.83	69.54
.6	10453.33	62.31	.6	13090.37	69.72
.7	10515.65	62.50	.7	13160.09	69.91
.8	10578.15	62.69	.8	13229.99	70.09
.9	10640.83	62.87	.9	13300.09	70.28
34.0	10703.70	63.06	38.0	13370.37	70.46
.1	10766.76	63.24	.1	13440.83	70.65
.2	10830.00	63.43	.2	13511.48	70.83
.3	10893.43	63.61	.3	13582.31	71.02
.4	10957.04	63.80	.4	13653.33	71.20
.5	11020.83	63.98	.5	13724.54	71.39
.6	11084.81	64.17	.6	13795.93	71.57
.7	11148.98	64.35	.7	13867.50	71.76
.8	11213.33	64.54	.8	13939.26	71.94
.9	11277.87	64.72	.9	14011.20	72.13
35.0	11342.59	64.91	39.0	14083.33	72.31
.1	11407.50	65.09	.1	14155.65	72.50
.2	11472.59	65.28	.2	14228.15	72.69
.3	11537.87	65.46	.3	14300.83	72.87
.4	11603.33	65.65	.4	14373.70	73.06
.5	11668.98	65.83	.5	14446.76	73.24
.6	11734.81	66.02	.6	14520.00	73.43
.7	11800.83	66.20	.7	14593.43	73.61
.8	11867.04	66.39	.8	14667.04	73.80
.9	11933.43	66.57	.9	14740.83	73.98

Table 4.—Contents of Slopes, for a slope of  $2\frac{1}{2}$  to 1, and for a length of 100 feet.

Depths.	Contents.	D.	Depths.	Contents.	D.
40.0	14814.51	74.17	44.0	17925.93	81.57
.1	14888.98	74.35	.1	18007.50	81.76
.2	14963.33	74.54	.2	18089.26	81.94
.3	15037.87	74.72	.3	18171.20	82.13
.4	15112.59	74.91	.4	18253.33	82.31
.5	15157.50	75.09	.5	18335.65	82.50
.6	15262.59	75.28	.6	18418.15	82.69
.7	15337.87	75.46	.7	18500.83	82.87
.8	15413.33	75.65	.8	18583.70	83.06
.9	15488.98	75.83	.9	18666,76	53.24
41.0	15564.81	76.02	45.0	18750.00	83.43
.1	15646.83	76.20	.1	18833.43	83.61
.2	15717.04	76.39	.2	18917.04	83.80
.3	15793.43	76.57	.3	19000.83	83.98
.4	15870.00	76.76	.4	19084.81	84.17
.5	15946.76	76.94	.5	19168.98	84.35
.6	16023.70	77.13	,6	19253.33	84.54
.7	16100.83	77.31	.7	19337.87	84.72
.8	16178.15	77,50	.8	19422.59	84.91
.9	16255.65	77.69	.9	19507.50	85.09
42.0	16333.33	77.87	46.0	19592.59	85.28
.1	16411.20	78.06	.1	19677.87	85.46
.2	16489.26	78.24	.2	19763.33	85.65
.3	16567.50	78.43	.3	19848.98	85.83
.4	16645.93	78.61	.4	19934.81	86.02
.5	16724.54	78.80	.5	20020.53	86.20
.6	16803.33	78.98	.6	20107.04	86.39
.7	16882.31	79.17	.7	20193.43	86.57
.8	16961.48	79.35	.8	20250.00	86.76
.9	17040.83	79.54	.9	20366.76	86.94
43.0	17120.37	79.72	47.0	20453.70	87.13
.1	17200.09	79.91	.1	20540.83	87.31
.2	17279.99	80.09	.2	20628.15	87.50
.3	17360.09	80.28	.3	20715.65	87.69
.4	17440.37	80.46	.4	20803.33	87.87
.5	17520.83	80.65	.5	20891.20	88.06
.6	17601.48	80.53	.6	20979.26	88.24
.7	17682.31	81.02	.7	21067.50	88.43
.8	17763.33	81.20	.8	21155.93	88.61
.9	17844.54	81.39	.9	21244.54	88.80

'able 4.—Contents of Slopes, for a slope of  $2\frac{1}{2}$  to 1, and for a length of 100 fect.

Depths.	Contents.	D.	Depths.	Contents.	D.
48.0	21333.33	88.98	52.0	25037.04	96.39
.1	21422.31	89.17	.1	25133.43	96.57
.2	21511.48	89.35	.2	25230.00	96.76
.3	21600.83	89.54	.3	25326.76	96,94
.4	21690.37	89.72	.4	25423.70	97.13
.5	21780.09	89.91	.5	25520.83	97.31
.6	21869.99	90.09	.6	25618.15	97.50
.7	21960.09	90.28	.7	25715.65	97.69
.8	22050.37	90.46	.8	25813.33	97.87
.9	22140.83	90.65	.9	25911.20	95.06
49.0	22231.48	90.83	53.0	26009.26	98.24
.1	22322.31	91.02	.1	26107.50	98.43
.2	22413.33	91.20	.2	26205.93	98.61
.3	22504.54	91.39	.3	26304.54	98.80
.4	22595.93	91.57	.4	26403.33	98.98
.5	22687.50	91.76	.5	26502.31	99.17
.6	22779.26	91.94	.6	26601.48	99.35
.7	22871.20	92.13	.7	26700.83	99.54
.S	22963.33	92.31	.8	26800.37	99.72
.9	23055.65	92.50	.9	26900.09	99.91
50.0	23148.15	92.69	54.0	27000.00	100.09
.1	23240.83	92.87	.1	27100.09	100.28
.2	23333.70	93.06	.2	27200.37	100.46
.3	23426.76	93.24	.3	27300.83	100.65
.4	23520.00	93.43	.4	27401.48	100.83
.5	23613.43	93.61	.5	27502.31	101.02
.6	23707.04	93.80	.6	27603.33	101.20
.7	23800.83	93.98	.7	27704.54	101.39
.8	23894.81	94.17	.8	27805.93	101.57
.9	23988.98	94.35	.9	27907.50	101.76
51.0	24083.33	94.54	55.0	28009.26	101.94
.1	24177.87	94.72	.1	28111.20	102.13
.2	24272.59	94.91	2	28213.33	102.31
.3	24367.50	95.09	.3	28315.65	102.50
.4	24462.59	95.28	.4	28418.15	102.69
.5	24557.87	95.46	.5	28520.83	102.87
.6	24653,33	95.65	.6	28623.70	103.06
.7	24748.98	95.83	.7	28726.76	103.24
.8	24844.81	96.02	.8	28830.00	103.43
.9	24940.83	96.20	.9	28933.43	103.61

Table 4.—Contents of Slopes, for a slope of  $2\frac{1}{2}$  to 1, and for a length of 100 feet.

Depths.	Contents.	D.	Depths.	Contents.	D.
56.0	29037.04	103.80	60.0	33333.33	111.20
.1	29140.83	103.98	.1	33444.54	111.39
.2	29244.81	104.17	.2	33555.93	111.57
.3	29348.98	104.35	.3	33667.50	111.76
.4	29453.33	104.54	.4	33779.26	111.94
.5	29557.87	104.72	.5	33891.20	112.13
.6	29662.59	104.91	.6	34003.33	112.31
.7	29767.50	105.09	.7	34115.65	112.50
.8	29872.59	105.28	.8	34228.15	112.69
.9	29977.87	105.46	.9	34340.83	112.87
57.0	30083.33	105.65	61.0	34453.70	113.06
.1	30188.98	105.83	.1	34566.76	113.24
.2	30294.81	106.02	.2	34680.00	113.43
.3	30400.83	106.20	.3	34793.43	113.61
.4	30507.04	106.39	.4	34907.04	113.80
.5	30613.43	106.57	.5	35020.83	113.98
.6	30720.00	106.76	.6	35134.81	114.17
.7	30826.76	106.94	.7	35248.98	114.35
.8	30933.70	107.13	.8	35363.33	114.54
.9	31040.83	107.31	.9	35477.87	114.72
58.0	31148.15	107.50	62.0	35592.59	114.91
.1	31255.65	107.69	.1	35707.50	115.09
.2	31363.33	107.87	.2	35822.59	115.28
.3	31471.20	108.06	.3	35937.87	115,46
.4	31579.26	108.24	.4	36053.33	115,65
.5	31687.50	108.43	.5	36168.98	115,83
.6	31795.93	108.61	.6	36284.81	116.02
.7	31904.54	108.80	.7	36400.83	116,20
.8	32013.33	108.98	.8	36517.04	116,39
.9	32122.31	109.17	.9	36633.43	116,57
59.0	32231.48	109.35	63.0	36750.00	116,76
.1	32340.83	109.54	.1	36866.76	116.94
.2	32450.37	109.72	.2	36983.70	117,13
.3	32560.09	109.91	.3	37100.83	117.31
.4	32670.00	110.09	.4	37218.15	117,50
.5	32780.09	110.28	.5	37335.65	117,69
.6	32890.37	110.46	.6	37453.33	117.87
.7	33000.83	110.65	.7	37571.20	118.06
.8	33111.48	110,83	.8	37689.26	118.24
.9	33222.31	111.02	.9	37807.50	118.43

Table 4.—Contents of Slopes, for a slope of  $2\frac{1}{2}$  to 1, and for a length of 100 feet.

Depths.	Contents.	D.	Depths.	Contents.	D.
-					
64.0	37925.92	118.61	68.0	42814.81	126.02
.1	38044.54 38163.33	118.80 118.98	.1	42940.83 43067.04	126.20
					126.39
.3	38282.31	119.17	.3	43193.43	126 57
.4	38401.48	119.35	.4	43320.00	126.76
.5	38520.83	119.54	.5	43446.76	126.94
.6	38640.37	119.72	.6	43573.70	127.13
.7	38760.09	119.91	.7	43700.83	127.31
.8	38880.00	120.09	.8	43828.15	127.50
.9	39000.09	120.28	.9	43955.65	127.69
65.0	39120.37	120.46	69.0	44083.33	127.87
.1	39240.83	120.65	.1	44211.20	128.06
.2	39361.48	120.83	.2	44339.26	128.24
.3	39482.31	121.02	.3	44467.50	128.43
.4	39603.33	121.20	.4	44595.93	128.61
.5	39724.54	121.39	.5	44724.54	128.80
.6	39845.93	121.57	.6	44853.33	128.98
.7	39967.50	121.76	.7	44982.31	129.17
.8	40089.26	121.94	.8	45111.48	129.35
.9	40211.20	122.13	.9	45240.83	129.54
66.0	40333.33	122.31	70.0	45370.37	129.72
.1	40455.65	122.50	.1	45500.09	129.91
.2	40578.15	122.68	.2	45630.00	130.09
.3	40700.83	122.87	.3	45760.09	130.28
.4	40823.70	123.06	.4	45890.37	130.46
.5	40946.76	123.24	.5	46020.83	130.65
.6	41070.00	123.43	.6	46151.48	130.83
.7	41193.43	123.61	.7	46282.31	131.02
.8	41317.04	123.80	.8	46413.33	131.20
.9	41440.83	123.98	.9	46544.54	131.39
67.0	41564.81	124.17	71.0	46675.93	131.57
.1	41688.98	124.35	.1	46807.50	131.76
.2	41813.33	124.54	.2	46939.26	131.94
.3	41937.87	124.72	.3	47071.20	132.13
.4	42062.59	124,91	.4	47203.33	132.31
.5	42187.50	125.09	.5	47335.65	132.50
.6	42312.59	125.28	.6	47468.15	132.69
.7	42437.87	125.46	.7	47600.83	132.87
.8	42563.33	125.65	.8	47733.70	133.06
.9	42688.98	125.83	.9	47866.76	133.24

Supplement to table 4.—Slope 2½ to 1.—Solid contents.

Length.	Depth.						
Len	0.1	0.2	0.3	0.4	0.5	Length.	
10	.01	.04	.08	.15	.23	10	
20	.02	.08	.16	.30	.46	20	
30	.03	.12	.24	.45	.69	30	
40	.04	.16	.32	.60	.92	40	
50	.05	.20	.40	.75	1.15	50	
60	.06	.24	.48	.90	1.38	60	
70	.07	.28	.56	1.05	1.61	70	
80	.08	.32	.64	1.20	1.84	80	
90	.09	.36	.72	1.35	2.07	90	
100	.10	.40	.80	1.50	2.30	100	
Length.	0.6	0.7	0.8	0.9	1.0	Length	
10	.33	.45	.59	.75	.93	10	
20	.66	.90	1.18	1.50	1.86	20	
30	.99	1.35	1.77	2.25	2.79	30	
40	1.32	1.80	2.36	3.00	3.72	40	
50	1.65	2.25	2.95	3.75	4.65	50	
60 '	1.98	2.70	3.54	4.50	5.58	60	
70	2.31	3.15	4.13	5.25	6.51	70	
80	264	3.60	4.72	6.00	7.44	80	
90	2.97	4.05	5.31	6.75	8.37	90	
100	3.30	4.50	5.90	7.50	9.30	100	
Length.	1.1	1.2	1.3	1.4	1.5	Length	
10	1.12	1.33	1.56	1.81	2.08	10	
20	2.24	2.66	3.12	3.62	4.16	20	
30	3.36	3.99	4.68	5.43	6.24	30	
40	4.48	5.32	6.24	7.24	8.32	40	
50	5.60	6.65	7.80	9.05	10.40	50	
60	<b>62.7</b>	7.98	9.36	10.86	12.48	60	
70	7.84	9.31	10.92	12.67	14.56	70	
80	8.96	10.64	12.48	14.48	16.64	80	
90	10.08	11.97	14.04	16.29	18.72	90	
100	11.20	13.30	15.60	18.10	20.80	100	

CONTENTS OF SLOPES.

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

gth.			Depth.			gth.
Length.	1.6	1.7	1.8	1.9	2.0	Length.
10	2.37	2.68	3.00	3.34	3.70	10
20	4.74	5.36	6.00	6.68	7.40	20
<b>3</b> 0	7.11	8.04	9.00	10.02	11.10	30
40	9.48	10.72	12.00	13.36	14.80	40
50	11.85	13.40	15.00	16.70	18.50	50
60	14.22	16.08	18.00	20.04	22.20	60
70	16.59	18.76	21.00	23.38	25.90	70
80	18.96	21.44	24.00	26.72	29.60	80
90	21.33	24.12	27.00	30.06	33.30	90
100	23.70	26.80	30.00	33.40	37.00	100
L.	2.1	2.2	2.3	2.4	2.5	L.
10	4.08	4.48	4.90	5.33	5.79	10
20	8.16	8.96	9.80	10.66	11.58	20
30	12.24	13.44	14.70	15.99	17.37	30
<b>4</b> 0	16.32	17.92	19.60	21.32	23.16	40
50	20.40	22.40	24.50	26.65	28.95	50
<b>6</b> 0	24.48	26.88	29.40	31.98	34.74	60
70	28.56	31.36	34.30	37.31	40.53	70
80	32.64	35.84	39.20	42.64	46.32	80
90	36.72	40.32	44.10	47.97	52.11	90
100	40.80	44.80	49.00	53.30	57.90	100
L.	2.6	2.7	2.8	2.9	3.0	L.
10	6.26	6.75	7.26	7.79	8.33	10
20	12.52	13.50	14.52	15.58	16.66	20
30	18.78	20.25	21.78	23.37	24.99	30
40	25.04	27.00	29.04	31.16	33.32	40
50	31.30	33.75	36.30	38.95	41.65	50
60	37.56	40.50	43.56	46.74	49.98	60
70	43.82	47.25	50.82	54.53	58.31	70
80	50.08	54.00	58.08	62.32	66.64	80
90	56.34	60.75	65.34	70.11	74.97	90
100	62.60	67.50	72.60	77.90	83.30	100
	10					

Supplement to table 4.—Slope 2½ to 1.—Solid contents.

Length.	Depth.						
Len	3.1	3.2	3.3	3.4	3.5	Length.	
10	8.90	9.48	10.08	10.70	11.34	10	
20	17.80	18.96	20.16	21.40	22.68	20	
30	26.70	28.44	30.24	32.10	34.02	30	
40	35.60	37.92	40.32	42.80	45.36	40	
<b>50</b>	44.50	47.40	<b>50.4</b> 0	53.50	56.70	50	
60	<b>53.4</b> 0	56.88	60.48	64.20	68.04	60	
70	62.30	66.36	70.56	74.90	79.38	70	
80	71.20	75.84	80.64	85.60	90.72	80	
90	80.10	85.32	90.72	96.30	102.06	90	
100	89.00	94.80	100.80	107.00	113.40	100	
L.	3.6	3.7	3.8	3.9	4.0	L.	
10	12.00	12.68	13.37	14.08	14.81	10	
20	24.00	25.36	26.74	28.16	29.62	20	
.30	36.00	38.04	40.11	42.24	44.43	30	
40	48.00	50.72	53.48	56.32	59.24	40	
<b>5</b> 0	60.00	63.40	66.85	70.40	74.05	50	
<b>6</b> 0	72.00	76.08	80.22	84.48	88.86	60	
70	84.00	88.76	93.59	98.56	103:67	70	
80	96.00	101.44	106.96	112.64	118.48	80	
90	108.00	114.12	120.33	126.72	133.29	90	
100	120.00	126.80	133.70	140.80	148.10	100	
L.	4.1	4.2	4.3	4.4	4.5	L.	
10	15.56	16.33	17.12	17.93	18.75	10	
20	31.12	32.66	34.24	35.86	37.50	20	
30	46.68	48.99	51.36	53.79	56.25	30	
40	62 24	65.32	68.48	71.72	75:00	40	
<b>50</b>	77.80	81.65	85.60	89.65	93.75	50	
60	93.36	97.98	102.72	107.58	112.50	60	
70	108.92	114.31	119.84	125.51	131.25	70	
80	124.48	130.64	136.96	143.44	150.00	80	
90	140.04	146.97	154.08	161.37	168.75	90	
100	155.60	163.30	171.20	179.30	187.50	100	

## CONTENTS OF SLOPES.

Supplement to table 4.—Slope 2½ to 1.—Solid contents.

gth.			Depth.			gth.
Length.	4.6	4.7	4.8	4.9	5.0	Length.
10	19.59	20.45	21 33	22.23	23.15	10
20	39.18	40.90	42.66	44.46	46.30	20
30	58.77	61.35	<b>63</b> .99	66.69	69.45	30
40	78.36	81.80	85.32	88.92	92.60	40
<b>5</b> 0	97.95	102 25	106 65	111.15	115.75	50
69	117.54	122.70	127.98	133.38	138 90	60
70	137.13	143.15	149.31	155.61	162.05	70
80	156.72	163.60	170.64	177.84	185.20	80
90	176.31	184.05	191 97	200.07	208.35	90
100	195.90	204.50	213.30	222.30	231.50	100
<b>L</b> .	5.1	5.2	5.3	5.4	5.5	L.
10	24.08	25.04	26.01	27.00	28.01	10
20	48.16	50.08	52.02	54.00	56.02	20
80	72.24	75 12	78.03	81.00	84.03	30
40	96.32	100.16	104.04	108.00	112.04	40
50	120.40	125.20	130.05	135.00	140.05	50
60	144.48	150.24	156.06	162.00	168.06	60
70	168.56	175.28	182.07	189.00	196.07	70
80	192.64	200.32	208.08	216.00	224.08	80
90	216.72	225.36	<b>234</b> .09	<b>243.0</b> 0	252.09	90
100	240.80	250.40	260.10	270.00	280.10	100
L.	5.6	5.7	5.8	5.9	6.0	L.
10	29.04	30.08	31.15	32.23	33.33	10
20	58.08	69.16	62.30	64.46	66.66	20
80	87.12	90.24	93.45	96.69	99.99	30
40	116.16	120.32	124 60	128.92	133.32	40
<b>5</b> 0	145.20	150.40	155.75	161.15	166.65	50
<b>6</b> 0	174.24	180.48	186.90	193.38	199.98	60
70	203.28	210.56	218.05	225.61	233.31	70
80	232.32	240.64	249.20	257.84	266.64	80
90	261.36	270.72	280.35	290.07	299.97	90
100	290.40	800.80	811.50	822.80	883.30	100

Supplement to table 4.—Slope 24 to 1.—Solid contents.

	<del></del>		<u>-</u>			
ż			Depth.			gth.
Length.	6.1	6.2	6.3	6.4	6.5	Length.
10	34.45	35.59	36.75	37.93	39.12	10
20	68.90	71.18	73.50	7á.86	78.24	20
<b>3</b> 0	103.35	106.77	110.25	113.79	117.36	30
40	137.80	142.36	147.00	151.72	156.48	40
<b>5</b> 0	172.25	177.95	183.75	189.65	195.60	50
60	206.70	213.54	220.50	227.58	234.72	60
70	241.15	249.13	257.25	265.51	273.84	70
80	275.60	284.72	294.00	303.44	312.96	80
90	310.05	320.31	330.75	341.37	352.08	90
100	344.50	355.90	367.50	379.30	391.20	100
L.	6.6	6.7	6.8	6.9	7.0	L.
10	40.33	41.56	42.81	44.08	45.37	10
20	80.66	83.12	85.62	88.16	90.74	20
30	120.99	124.68	128.43	132.24	136.11	30
40	161.32	166.24	171.24	176.32	181.48	40
<b>5</b> 0	201.65	207.80	214.05	220.40	226.85	50
60	241.98	249.36	256.86	264.48	272.22	60
70	282.31	290.92	299.67	308.56	317.59	70
80	322.64	332.48	342.48	352.64	362.96	80
90	362.97	374.04	385.29	396.72	408.33	90
100	403.30	415.60	428.10	440.80	453.70	100
<i>L</i> .	7.1	7.2	7.3	7.4	7.5	L.
10	46.68	48.00	49.34	50.70	52.08	10
20	93.36	96.00	98.68	101.40	104.16	20
30	140.04	144.00	148.02	152.10	156.24	30
40	186.72	192.00	197.36	202.80	208.32	40
<b>5</b> 0	233.40	240.00	246.70	253.50	<b>26</b> 0. <b>40</b>	50
<b>6</b> 0	280.08	288.00	296.04	304.20	312.48	60
70	326.76	3 <b>36</b> .00	345.38	354.90	364.56	70
80	373.44	384.00	394.72	405.60	416.64	80
90	420.12	432.00	444.06	456.30	468.72	90
100	466.80	480.00	493.40	507.00	<b>520.80</b>	100

CONTENTS OF SLOPES.

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

gth.			Depth.			gth.
Length.	7.6	7.7	7.8	7.9	8.0	Length.
10	53.48	54.90	56.33	57.79	59.26	10
20	106.96	109.80	112.66	115.58	118.52	20
30	160.44	164.70	168.99	173.37	177.78	30
40	213.92	219.60	225.32	231.16	237.04	40
50	267.40	274.50	281.65	288.95	296.30	50
60	320.88	329.40	337.98	346.74	355.56	60
70	374.36	384.30	394.31	404.53	414.82	70
80	427.84	439.20	450.64	462.32	474.08	80
90	481.32	494.10	506.97	520.11	533.34	90
100	534.80	549.00	563.30	577.90	592.60	100
L.	8.1	8.2	8.3	8.4	8.5	L.
10	60.75	62.26	63.79	65.33	66.90	10
20	121.50	124.52	127.58	130.66	133.80	20
30	182.25	186.78	191.37	195.99	200.70	30
40	243.00	249.04	255.16	261.32	267.60	40
<b>5</b> 0	303.75	311.30	318.95	326.65	334.50	50
60	364.50	373.56	382.74	391.98	401.40	60
70	425.25	435.82	446.53	457.31	468.30	70
80	486.00	498.08	510.32	522.64	535.20	80
<b>90</b>	546.75	560.34	574.11	587.97	602.10	90
100	607.50	622.60	637.90	653.30	669.00	100
L.	8.6	8.7	8.8	8.9	9.0	L.
10	68,48	70.08	71.70	73.34	75.00	10
20	136.96	140.16	143.40	146.68	150.00	20
30	205.44	210.24	215.10	220.02	225.00	30
40	273.92	280.32	286.80	293.36	300.00	40
50	342.40	350.40	358.50	366.70	375.00	50
60	410.88	420.48	430.20	440.04	450.00	60
70	479.36	490.56	501.90	513.38	525.00	70
80	547.84	560.64	573.60	586.72	600.00	80
90	616.32	630.72	645.30	660.06	675.00	90
100	684.80	700.80	717.00	733.40	750.00	100

Supplement to table 4.—Slope 2½ to 1.—Solid contents.

gth.			Depth.			gth.
Length.	9.1	9.2	9.3	9.4	9.5	Length.
10	76.68	78.37	80.08	81.81	83.56	10
20	153.36	156.74	169.16	163.62	167.12	20
30	230.04	235.11	240.24	245.43	250 68	30
40	30 <i>5</i> .72	313.48	320.32	327.24	334.24	40
<b>5</b> 0	383.40	391.85	400.40	409.05	417.80	50
60	469.08	470.22	480.48	490.86	501.36	60
<b>7</b> 0	536.76	548.59	560.5 <b>6</b>	572.67	584.92	70
80	613.44	626.96	640.64	654.48	668.48	80
90	690.12	705.33	720.72	736.29	752.04	90
100	766.80	783.70	800.80	818.10	835.60	100
L.	9.6	9.7	9.8	9.9	10.0	<b>L</b> .
10	85.33	87.12	88.93	90.75	92.59	10
20	170.66	174.24	177.86	181.50	185.18	20
30	255.99	261.36	266.79	272.25	277.77	30
40	341.32	348.48	355.72	363 00	370.36	40
50	426.65	435 60	444.65	453.75	462.95	50
60	511.98	522.72	533.58	544.50	555.54	60
70	597.31	609.84	622.51	635.25	648.13	70
80	682.64	696.96	711.44	726.00	740.72	80
90	767.97	784.08	800.37	816.75	833.31	90
100	853.30	871.20	889.30	907.50	925.90	100
L.	10.1	10.2	10.3	10.4	10.5	L.
10	94.45	96.33	98.23	100.15	102.08	10
20	188.90	192.66	196 46	200.30	204.16	20
30	283.35	288.99	294.69	300.45	306 24	30
40	377.80	385.32	392.92	400.60	408.32	40
50	472.25	481.65	491.15	500.75	510.40	50
<b>6</b> 0	566.70	577.98	589.38	600.90	612.48	60
70	661.15	674.31	687.61	701.05	714.56	70
80	755.60	770.64	785.84	801.20	816.64	80
90	850.05	866.97	884.07	901.35	918.72	90
100	944.50	963.30	982.30	1001 50	1020.80	100

Supplement to table 4.—Slope 2½ to 1.—Solid contents.

* ;		<b>D</b> e	pth.		th.
: \$	10.6	10.7	. 10.8	10.9	Length.
P-10	104.04	106.01	108.00	110.01	10
E. <b>30</b> 0	208.08	212.02	216.00	220.02	20
	312.12	318.03	324.00	330.03	30
==40	416.16	424.04	432.00	440.04	40
<b>-#50</b>	520.20	530.05	540.00	550.05	50
<b>-40</b>	624.24	636.06	648.00	660.06	60
<b>=†</b> 0	728.28	742.07	756.00	770.07	70
<b>≇</b> ∲0	832.32	848.08	864.00	880.08	80
<b>2 9</b> 0	936.36	954.09	972.00	990.09	90
<b>∌₩</b> 0	1040.40	1060.10	1080.00	1100.10	100
. <b>L</b> .	11.0	11.1	11.2	11.3	<b>L</b> .
-110	112.04	114.08	116.15	118.23	10
<b>\$2</b> 0	224.08	228.16	232.30	236.46	20
<b>#3</b> 0	336.12	342.24	348.45	354.69	30
<b>±40</b>	448.16	456.32	464.60	472.92	40
<b>₹50</b>	560.20	570.40	580.75	591.15	50
<b>6</b> 0	672.24	684.48	696.90	709.38	60
<b>-</b> 70	784.28	798.56	813.05	827.61	70
<b>≱</b> 80	896.32	912.64	929.20	945.84	80
<b>()</b> 90	1008.36	1026.72	1045.35	1064.07	90
- <b>10</b> 0	1120.40	1140.80	1161.50	1182.30	100
L.	11.4	11.5	11.6	11.7	<b>L</b> .
10	120.33	122.45	124.59	126.75	10
20	240.66	244.90	249.18	253.50	20
80	360.99	367.35	373.77	380.25	30
40	481.32	489.80	498.36	507.00	40
<b>5</b> 0	601.65	612.25	622.95	633.75	50
60	721.98	734.70	747.54	760.50	60
70	842.31	857.15	872.13	887.25	70
80	962.64	979.60	996.72	1014.00	80
90	1082.97	1102.05	1121.31	1140.75	90
100	1203.30	1224.50	1245.90	1267.50	100

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

th.		•	Dcpth.			gth.
Length.	9.1	9.2	9.3	9.4	9.5	Length.
10	76.68	78.37	80.08	81.81	83.56	10
20	153.36	156.74	169.16	163.62	167.12	20
30	230.04	235.11	240.24	245.43	250 68	30
40	30ა.72	313.48	320.32	327.24	334.24	40
<b>5</b> 0	383.40	391.85	400.40	409.05	417.80	50
60	469.08	470.22	480.48	490.86	501.36	60
70	536.76	548.59	560.56	572.67	584.92	70
80	613.44	626.96	640.64	654.48	668.48	80
90	690.12	705.33	720.72	736.29	752.04	90
100	766.80	783.70	800.80	818.10	835.60	100
<i>L</i> .	9.6	9.7	9.8	9.9	10.0	L.
10	85.33	87.12	88.93	90.75	92.59	10
20	170.66	174.24	177.86	181.50	185.18	20
30	255.99	261.36	266.79	272.25	277.77	30
40	341.32	348.48	355,72	363 00	370.36	40
50	426.65	435 60	444.65	453.75	462.95	50
60	511.98	522.72	533.58	544.50	555.54	60
70	597.31	609.84	622.51	635.25	648.13	70
80	682.64	696.96	711.44	726.00	740.72	80
90	767.97	784.08	800.37	816.75	833.31	90
100	853.30	871.20	889.30	907.50	925.90	100
<i>L</i> .	10.1	10.2	10.3	10.4	10.5	L.
10	94.45	96.33	98.23	100.15	102.08	10
20	188.90	192.66	196 46	200.30	204.16	20
30	283.35	288.99	294.69	300.45	306 24	30
40	377.80	385.32	392.92	400.60	408.32	40
50	472.25	481.65	491.15	500.75	510.40	50
<b>6</b> 0	566.70	577.98	589.38	600.90	612.48	60
70	661.15	674.31	687.61	701.05	714.56	70
80	755.60	770.64	785.84	801.20	816.64	80
90	850.05	866.97	884.07	901.35	918.72	90
100	944.50	963.30	982.30	1001 50	1020.80	100

CONTENTS OF SLOPES.

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

gth.		Depth.					
Length.	10.6	10.7	. 10.8	10.9	Length.		
10	104.04	106.01	108.00	110.01	10		
20	208.08	212.02	216.00	220.02	20		
30	312.12	318.03	324.00	330.03	30		
40	416.16	424.04	432.00	440.04	40		
50	<b>520.20</b>	530.05	540.00	550.05	50		
60	624.24	636.06	648.00	660.06	60		
70	728.28	742.07	756.00	770.07	70		
80	832.32	848.08	864.00	880.08	80		
90	936.36	954.09	972.00	990.09	90		
100	1040.40	1060.10	1080.00	1100.10	100		
L.	11.0	11.1	11.2	11.3	<i>L</i> .		
10	112.04	114.08	116.15	118.23	10		
20	224.08	228.16	232.30	236.46	20		
30	336.12	342.24	348.45	354.69	30		
40	448.16	456.32	464.60	472.92	40		
<b>5</b> 0	560.20	570.40	580.75	591.15	50		
60	672.24	684.48	696.90	709.38	60		
70	784.28	798.56	813.05	827.61	70		
80	896.32	912.64	929.20	945.84	80		
90	1008.36	1026.72	1045.35	1064.07	90		
100	1120.40	1140.80	1161.50	1182.30	100		
.L.	11.4	11.5	11.6	11.7	<b>L</b> .		
10	120.33	122.45	124.59	126.75	10		
20	240.66	244.90	249.18	253.50	20		
30	360.99	367.35	373.77	380.25	30		
40	481.32	489.80	498.36	507.00	40		
<b>5</b> 0	601.65	612.25	622.95	633.75	50		
60	721.98	734.70	747.54	760.50	60		
70	842.31	857.15	872.13	887.25	70		
80	962.64	979.60	996.72	1014.00	80		
90	1082.97	1102.05	1121.31	1140.75	90		
100	1203.30	1224.50	1245.90	1267.50	100		

Supplement to table 4.—Slope 2½ to 1.—Solid contents.

gth.		Depth.					
Length.	11.8	11.9	12.0	12.1	Length.		
10	128.93	131.12	133.33	135.56	10		
20	<b>257.8</b> 6	262.24	266.66	271.12	20		
30	386.79	393.36	<b>399</b> .99	406.68	30		
40	515.72	524.48	533.32	542.24	40		
50	644.65	655.60	666.65	677.80	50		
60	773.58	786.72	799.98	813.36	60		
70	902.51	917.84	933.31	948.92	70		
80	1031.44	1048.96	1066.64	1084.48	80		
90	1160.37	1180.08	1199.97	1220.04	90		
100	1289.30	1311.20	1333.30	1355.60	100		
<b>L</b> .	12.2	12.3	12.4	12.5	L.		
10	137.81	140.08	142.37	144.68	10		
20	275.62	280.16	284.74	289.36	20		
30	413.43	420.24	427.11	434.04	30		
40	551.24	560.32	569.48	578.72	40		
50	689.05	700.40	711.85	723.40	50		
60	826.86	840.48	854.22	868.08	60		
70	964.67	980.56	<b>996</b> .59	1012.76	70		
80	1102.48	1120.64	1138.96	1157.44	80		
90	1240.29	1260.72	1281.33	1302.12	90		
100	1378.10	1400.80	1423.70	1446.80	100		
<b>L</b> .	12.6	12.7	12.8	12.9	L.		
10	147.00	149.34	151.70	154.08	10		
20	294.00	298.68	303.40	308.16	20		
30	441.00	448.02	455.10	462.24	30		
40	588.00	597.36	606.80	616.32	40		
50	735.00	746.70	758.50	770.40	50		
60	882.00	896.04	910.20	924.48	60		
70	1029.00	1045.38	1061.90	1078.56	70		
80	1176.00	1194.72	1213.60	1232.64	80		
90	1323.00	1344.06	1365.30	1386.72	90		
100	1470.00	1493.40	1517.00	1540.80	100		

CONTENTS OF SLOPES.

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

gth.		Dep	oth.		gth.
Length.	13.0	13.1	13.2	13.3	Length.
10	156.48	158.90	161.33	163.79	10
20	312.96	317.80	322.66	327.58	20
30	469.44	476.70	483.99	491.37	30
40	625.92	635.60	645.32	655.16	40
50	782.40	794.50	806.65	818,95	50
60	938.88	953.40	967.98	982.74	60
70	1095.36	1112.30	1129.31	1146.53	70
80	1251.84	1271.20	1290.64	1310.32	80
90	1408.32	1430.10	1451.97	1474.11	90
100	1564.80	1589.00	1613.30	1637.90	100
L.	13.4	13.5	13.6	13.7	<b>L</b> .
10	166.26	168.75	171.26	173.79	10
20	332.52	337.50	342.52	347.58	20
30	498.78	506.25	513.78	521.37	30
40	665.04	675.00	685.04	695.16	40
50	831.30	843.75	856.30	868.95	50
60	997.56	1012.50	1027.56	1042.74	60
70	1163.82	1181.25	1198.82	1216.53	70
80	1330.08	1350.00	1370.08	1390.32	80
90	1496.34	1518.75	1541.34	1564.11	90
100	1662.60	1687.50	1712.60	1737.90	100
<i>L</i> .	13.8	13.9	14.0	14.1	<i>L</i> .
10	176.33	178.90	181.48	184.08	10
20	352.66	357.80	362.96	368.16	20
30	528.99	536.70	544.44	552.24	30
40	705.32	715.60	725.92	736.32	40
50	881.65	894.50	907.40	920.40	50
60	1057.98	1073.40	1088.88	1104.48	60
70	1234.31	1252.30	1270.36	1288.56	70
80	1410.64	1431.20	1451.84	1472.64	80
90	1586.97	1610.10	1633.32	1656.72	90
100	1763.30	1789.00	1814.80	1840.80	100

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

gth.	Depth.						
Length.	14.2	14.3	14.4	14.5	Length.		
10	186.70	189.34	192.00	194.68	10		
20	373.40	378.68	384.00	389.36	20		
30	560.10	568.02	576.00	584.04	30		
40	746.80	757.36	768.00	778.72	40		
<b>5</b> 0	933.50	946.70	960.00	973.40	50		
60	1120.20	1136.04	1152.00	1168.08	60		
70	1306.90	1325.38	1344.00	1362.76	70		
80	1493.60	1514.72	1536.00	1557.44	80		
90	1680.30	1704.06	1728.00	1752.12	90		
100	1867.00	1893.40	1920.00	1946.80	100		
L.	14.6	14.7	14.8	14.9	<b>L</b> .		
10	197.37	200.08	202.81	205.56	10		
20	394.74	400.16	405.62	411.12	20		
30	592.11	600.24	608.43	616.68	30		
40	789.48	800.32	811.24	822.24	40		
<b>50</b>	986.85	1000.40	1014.05	1027.80	50		
<b>6</b> 0	1184.22	1200.48	1216.86	1233.36	60		
70	1381.59	1400.56	1419.67	1438.92	70		
80	1578.96	1600.64	1622.48	1644.48	80		
90	1776.33	1800.72	1825.29	1850.04	90		
100	1973.70	2000.80	2028.10	2055.60	100		
L.	15.0	15.1	15.2	15.3	L.		
10	208,33	211.12	213.93	216.75	10		
20	416.66	422.24	427.86	433.50	20		
30	624,99	633.36	641.79	650.25	30		
40	833.32	844.48	855.72	867.00	40		
<b>5</b> 0	1041.65	1055.60	1069.65	1083.75	50		
60	1249.98	1266.72	1283.58	1300.50	60		
70	1458.31	1477.84	1497.51	1517.25	70		
80	1666.64	1688.96	1711.44	1734.00	80		
90	1874.97	1900.08	1925.37	1950.75	90		
100	2083.30	2111.20	2139.30	2167.50	100		

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

gth.		De	pth.		gth.
Length.	15.4	15.5	15.6	15.7	Length.
10	219.59	222.45	225.33	228.23	10
20	439.18	444.90	450.66	456.46	20
30	658.77	667.35	675.99	684.69	30
40	878.36	889.80	901.32	912.92	40
50	1097.95	1112.25	1126.65	1141.15	50
60	1317.54	1334.70	1351.98	1369.38	60
70	1537.13	1557.15	1577.31	1597.61	70
80	1756.72	1779.60	1802.64	1825.84	80
90	1976.31	2002.05	2027.97	2054.07	90
100	2195.90	2224.50	2253.30	2282.30	100
<b>L</b> .	15.8	15.9	16.0	16.1	<b>L</b> .
10	231.15	234.08	237.04	240.01	10
20	462.30	468.16	474.08	480.02	20
30	693.45	702.24	711.12	720.03	30
40	924.60	936.32	948.16	960.04	40
50	1155.75	1170.40	1185.20	1200.05	50
60	1386.90	1404.48	1422.24	1440.06	60
70	1618.05	1638.56	1659.28	1680.07	70
80	1849.20	1872.64	1896.32	1920.08	80
90	2080.35	2106.72	2133.36	2160.09	90
100	2311.50	2340.80	2370.40	2400.10	100
L.	16.2	16.3	16.4	16.5	<b>L</b> .
10	243.00	246.01	249.04	252.08	10
20	486.00	492.02	498.08	504.16	20
30	729.00	738.03	747.12	756.24	30
40	972.00	984.04	996.16	1008.32	40
50	1215.00	1230.05	1245.20	1260.40	50
60	1458.00	1476.06	1494.24	1512.48	60
70	1701.00	1722.07	1743.28	1764.56	70
80	1944.00	1968.08	1992.32	2016.64	80
90	2187.00	2214.09	2241.36	2268.72	90
100	2430.00	2460.10	2490.40	2520.80	100

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

	11		<u> </u>		
Length.		Dep	oth.		Length.
Len	16.6	16.7	16.8	16.9	Len
10	255.15	258.23	261.33	264.45	10
20	510.30	516.46	522.66	528.90	20
30	765.45	774.69	783.99	793.35	30
. <b>40</b>	1020.60	1032.92	1045.32	1057.80	40
50	1275.75	1291.15	1306 65	1322.25	50
60	1530.90	1549.38	1567.98	1586.70	60
70	1786.05	1807.61	1829.31	1851.15	70
80	2041.20	2065.84	2090.64	2115.60	80
90	2296.35	2324.07	2351.97	2380.05	90
100	2551.50	2582.30	2613.30	2644.50	100
<b>L</b> .	17.0	17.1	17.2	17.3	<b>L</b> .
10	267.59	270.75	273.93	277.12	10
20	535.18	541.50	547.86	554.24	20
30	802.77	812.25	821.79	831.36	30
40	1070.36	1083.00	1095.72	1108.48	40
50	1337.95	1353.75	1369.65	1385.60	50
60	1605.54	1624.50	1643.58	1662.72	60
70	1873.13	1895.25	1917.51	1939.84	70
80	2140.72	2166.00	2191.44	2216.96	80
90	2408.31	2436.75	2465.37	2494.08	90
100	2675.90	2707.50	2739.30	2771.20	100
L.	17.4	17.5	17.6	17.7	L.
10	280.33	283.56	286.81	290.08	10
20	560.66	567.12	573.62	580.16	20
30	840.99	850.68	860.43	870.24	30
40	1121.32	1134.24	1147.24	1160.32	40
<b>50</b>	1401.65	1417.80	1434.05	1450.40	50
60	1681.98	1701.36	1720.86	1740.48	60
70	1962.31	1984.92	2007.67	2030.56	70
80	2242.64	2268.48	2294.48	2320.64	80
90	2522,97	2552.04	2581.29	2610.72	90
100	2803.30	2835.60	2868.10	2900.80	100

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

th.			pth.		th.
Length.	17.8	17.9	18.0	18.1	Length.
10	293.37	296.68	300.00	303.34	10
20	586.74	593.36	600.00	606.68	20
30	880.11	890.04	900.00	910.02	30
40	1173.48	1186.72	1200.00	1213.36	40
50	1466.85	1483.40	1500.00	1516.70	50
60	1760.22	1780.08	1800.00	1820.04	60
70	2053.59	2076.76	2100.00	2123.38	70
80	2346.96	2373.44	2400.00	2426.72	80
90	2640.33	2670.12	2700.00	2730.06	90
100	2933.70	2966.80	3000.00	3033.40	100
<i>L</i> .	18.2	18.3	18.4	18.5	L.
10	306.70	310.08	313.48	316.90	10
20	613.40	620.16	626.96	633.80	20
30	920.10	930.24	940.44	950.70	30
40	1226.80	1240.32	1253.92	1267.60	40
<b>50</b>	1533.50	1550.40	1567.40	1584.50	50
60	1840.20	1860.48	1880.88	1901.40	60
70	2146.90	2170.56	2194.36	2218.30	70
80	2453.60	2480.64	2507.84	2535.20	80
90	2760.30	2790.72	2821.32	2852.10	90
100	3067.00	3100.80	3134.80	3169.00	100
L.	18.6	18.7	18.8	18.9	<b>L</b> .
10	320.33	323.79	327.26	330.75	10
20	640.66	647.58	654.52	661.50	20
30	960.99	971.37	981.78	992.25	30
40	1281.32	1295.16	1309.04	1323.00	40
50	1601.65	1618.95	1636.30	1653.75	50
60	1921.98	1942.74	1963.56	1984.50	60
70	2242.31	2266.53	2290.82	2315.25	70
80	2562.64	2590.32	2618.08	2646.00	80
90	2882.97	2914.11	2945.34	2976.75	90
100	3203.30	3237.90	3272.60	3307.50	100

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

gth.		Dep	oth.		gth.
Length.	19.0	19.1	19.2	19.3	Length.
10	334.26	337.79	341.33	344.90	10
20	668.52	675.58	• 682.66	689.80	20
30	1002.78	1013.37	1023.99	1034.70	30
40	1337.04	1351.16	1365.32	1379.60	40
50	1671.30	1688.95	1706.65	1724.50	50
60	2005.56	2026.74	2047.98	2069.40	60
70	2339.82	2364.53	2389.31	2414.30	70
80	2674.08	2702.32	2730.64	2759.20	80
80	3008.34	3040.11	3071.97	3104.10	90
100	3342.60	3377.90	3413.30	3449.00	100
<b>L</b> .	19.4	19.5	19.6	19.7	<b>L</b> .
10	348.48	352.08	355.70	359.34	10
20	696.96	704.16	711.40	718.68	20
30	1045.44	1056.24	1067.10	1078.02	30
40	1393.92	1408.32	1422.80	1437.36	40
50	1742.40	1760.40	1778.50	1796.70	50
60	2090.88	2112.48	2134.20	2156.04	60
70	2439.36	2464.56	2489.90	2515.38	70
80	2787.84	2816.64	2845.60	2874.72	80
80	3136.32	3168.72	3201.30	3234.06	90
100	3484.80	3520.80	3557.00	3593.40	100
<i>L</i> .	19.8	19.9	20.0	20.1	L.
10	363.00	366.68	370.37	374.08	10
20	726.00	733.36	740.74	748.16	20
30	1089.00	1100.04	1111.11	1122.24	30
40	1452.00	1466.72	1481.48	1496.32	40
50	1815.00	1833.40	1851.85	1870.40	50
60	2178.00	2200.08	2222.22	2244.48	60
70	2541.00	2566.76	2592.59	2618.56	70
80	2904.00	2933.44	2962.96	2992.64	80
90	3267.00	3800.12	3333.33	3366.72	90
100	3630.00	<b>3666.80</b>	3703.70	3740.80	100

Supplement to table 4.—Slope 2½ to 1.—Solid contents.

gth.		Dep	oth.		th.
Length.	20.2	20.3	20.4	20.5	Length.
10	377.81	381.56	385.33	389.12	10
20	755.62	763.12	770.66	778.24	20
30	1133.43	1144.68	1155.99	1167.36	30
40	1511.24	1526.24	1541.32	1556.48	40
50	1889.05	1907.80	1926.65	1945.60	50
60	2266.86	2289.36	2311.98	2334.72	60
70	2644.67	2670.92	2697.31	2723.84	70
80	3022.48	3052.48	3082.64	3112.96	80
90	3400.29	3434.04	3467.97	3502.08	90
100	3778.10	3815.60	3853.30	3891.20	100
L.	20.6	20.7	20.8	20.9	<b>L</b> .
10	392.93	396.75	400.59	404.45	10
20	785.86	793.50	801.18	808.90	20
30	1178.79	1190.25	1201.77	1213.35	30
40	1571.72	1587.00	1602.36	1617.80	40
50	1964.65	1983.75	2002.95	2022.25	50
60	2357.58	2380.50	2403.54	2426.70	60
70	2750.51	2777.25	2804.13	2831.15	70
80	3143.44	3174.00	3204.72	3235.60	80
90	3536.37	3570.75	3605.31	3640.05	90
100	3929.30	3967.50	4005.90	4044.50	100
<b>L</b> .	21.0	21.1	21.2	21.3	<b>L</b> .
10	408.33	412.23	416.15	420.08	10
20	816.66	824.46	832.30	840.16	20
30	1224.99	1236.69	1248.45	1260.24	30
40	1633.32	1648.92	1664.60	1680.32	40
50	2041.65	2061.15	2080.75	2100.40	50
60	2449.98	2473.38	2496.90	2520.48	60
70	2858.31	2885.61	2913.05	2940.56	70
80	3266.64	3297.84	3329.20	3360.64	80
90	3674.97	3710.07	3745.35	3780.72	90
100	4083.30	4122.30	4161.50	4200.80	100

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

gth.		De	epth.		Length.
Length.	21.4	21.5	21.6	21.7	Len
10	424.04	428.01	432.00	436.01	10
20	848.08	856.02	864.00	872.02	20
30	1272.12	1284.03	1296.00	1308.03	30
40	1696.16	1712.04	1728.00	1744.04	40
<b>50</b>	2120.20	2140.05	2160.00	2180.05	50
<b>6</b> 0	2544.24	2568.06	2592.00	2616.06	60
70	2968.28	2996.07	3024.00	3052.07	70
80	3392.32	3424.08	3456.00	3488.08	80
90	3816.36	3852.09	3888.00	3924.09	. 90
100	4240.40	4280.10	4320.00	4360.10	100
L.	21.8	21.9	22.0	22.1	L.
10	440.04	444.08	448.15	452.23	10
20	880.08	888.16	896.30	904.46	20
30	1320.12	1332.24	1344.45	1356.69	30
40	1760.16	1776.32	1792.60	1808.92	40
<b>50</b>	2200.20	2220.40	2240.75	2261.15	50
60	2640.24	2664.48	2688.90	2713.38	60
70	3080.28	3108.56	3137.05	3165.61	70
80	3520.32	3552.64	3585.20	3617.84	80
90	3960.36	3996.72	4033.35	4070.07	90
100	4400.40	4440.80	4481.50	4522.30	100
<i>L</i> .	22.2	22.3	22.4	22.5	L.
10	456.33	460.45	464.59	468.75	10
20	912.66	920.90	929.18	937.50	20
30	1368.99	1381.35	1393.77	1406.25	30
40	1825.32	1841.80	1858.36	1875.00	40
50	2281.65	2302.25	- 2322.95	2343.75	50
60	2737.98	2762.70	2787.54	2812.50	60
70	3194.31	3223.15	3252.13	3281.25	70
80	<b>36</b> 50.64	3683.60	3716.72	, 3750.00	80
90	4106.97	4144.05	4181.31	4218.75	90
100	4563.30	4604.50	4645.90	4687.50	100

CONTENTS OF SLOPES.

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

Length.		Dep	oth.		gth.
Len	22.6	22.7	22.8	22.9	Length.
10	472.93	477.12	481.33	485.56	10
20	945.86	954.24	962.66	971.12	20
30	1418.79	1431.36	1443.99	1456.68	30
40	1891.72	1908.48	1925.32	1942.24	40
50	2364.65	2385.60	2406.65	2427.80	50
60	2837.58	2862.72	2887.98	2913.36	60
70	3310.51	3339.84	3369.31	3398.92	70
80	3783.44	3816.96	3850.64	3884.48	80
90	4256.37	4294.08	4331.97	4370.04	90
100	4729.30	4771.20	4813.30	4855.60	100
L.	23.0	23.1	23.2	23.3	L.
10	489.81	494.08	498.37	502.68	10
20	979.62	988.16	996.74	1005.36	20
30	1469.43	1482.24	1495.11	1508.04	30
40	1959.24	1976.32	1993.48	2010.72	40
50	2449.05	2470.40	2491.85	2513.40	50
60	<b>2938.86</b>	2964.48	2990.22	3016.08	60
70	3428.67	3458.56	3488.59	3518.76	70
80	3918.48	3952.64	3986.96	4021.44	80
90	4408.29	4446.72	4485.33	4524.12	90
100	4898.10	4940.80	4983.70	5026.80	100
<b>L</b> .	23.4	23.5	23.6	23.7	L.
10	507.00	511.34	515.70	520.08	10
20	1014.00	1022.68	1031.40	1040.16	20
30	1521.00	1534.02	1547.10	1560,24	30
40	2028.00	2045.36	2062.80	2080.32	40
50	2535.00	2556.70	2578.50	2600.40	50
60	3042.00	3068.04	3094.20	3120,48	60
70	3549.00	3579.38	3609.90	3640.56	70
80	4056.00	4090.72	4125.60	4160.64	80
90	<b>4563</b> .00	4602.06	4641.30	4680.72	90
100	5070.00	5113.40	5157.00	5200.80	100

Supplement to table 4.—Slope  $2\frac{1}{2}$  to 1.—Solid contents.

£th.		Depth.				
Length.	23.8	23.9	2 0	24.1	Length.	
10	524.48	528.90	533.33	537.79	10	
20	1048.96	1057.80	1066.66	1075.58	20	
30	1573.44	1586.70	1599.99	1613.37	30	
40	2097.92	2115.60	2133.32	2151.16	40	
50	2622.40	2644.50	2666.65	2688.95	50	
60	3146.88	3173.40	3199.98	3226.74	60	
70	3671.36	3702.30	3733.31	3764.53	70	
80	4195.84	4231.20	4266.64	4302.32	80	
90	4720.32	4760.10	4799.97	4840.11	90	
100	5244.80	5289.00	5333.30	5377.90	100	
<i>L</i> .	24.2	24.3	24.4	24.5	<b>L</b> .	
10	542.26	546.75	551.26	555.79	10	
20	1084.52	1093.50	1102.52	1111.58	20	
30	1626.78	1640.25	1653.78	1667.37	30	
40	2169.04	2187.00	2205.04	2223.16	40	
50	2711.30	2733.75	2756.30	2778.95	50	
60	3253.56	3280.50	3307.56	3334.74	60	
70	3795.82	3827.25	3858.82	3890.53	70	
80	4338.08	4374.00	4410.08	4446.32	80	
90	4880.34	4920.75	4961.34	5002.11	90	
100	5422.60	5467.50	5512.60	5557.90	100	
L.	24.6	24.7	24.8	24.9	L.	
10	560.33	564.90	569.48	574.08	10	
20	1120.66	1129.80	1138.96	1148.16	20	
30	1680.99	1694.70	1708.44	1722.24	30	
40	2241.32	2259.60	2277.92	2296.32	40	
<b>5</b> 0	2801.65	2824.50	2847.40	2870.40	50	
<b>6</b> 0	3361.98	3389.40	3416.88	3444.48	60	
70	3922.31	3954.30	3986.36	4018.56	70	
80	4482.64	4519.20	4555.84	4592.64	80	
80	5042.97	5084.10	5125.32	5166.72	90	
100	5603.30	5649.00	5694.80	5740.80	100	

Supplement to table 4.—Slope 2½ to 1.—Solid contents.

gth:		Depth.			
Length.	25.0	25.1	25.2	25.3	Length.
10	578.70	583.34	588.00	592.68	10
20	1157.40	. 1166.68	1176.00	1185.36	20
<b>30</b> ,	1736.10	1750.02	1764.00	1778.04	30
40	2314.80	2333.36	2352.00	2370.72	40
<b>5</b> 0	2893.50	2916.70	2940.00	2963.40	50
<b>6</b> 0	3472.20	3500.04	3528.00	3556.08	60
70	4050.90	4083.38	4116.00	4148.76	70
80	4629.60	4666.72	4704.00	4741.44	80
90	5208.30	5250.06	5292.00	5334.12	90
100	5787.00	5833.40	5880.00	5926.80	100
L.	25.4	25.5	25.6	25.7	<b>L</b> .
10	597.37	602.08	606.81	611.56	10
20	1194.74	1204.16	1213 62	1223.12	20
30	1792.11	1806.24	1820.43	1834.68	30
40	2389.48	2408.32	2427.24	2446 24	40
50	2986.85	3010.40	3034.05	3057.80	50
<b>6</b> 0	3584.22	3612.48	3640.86	3669.36	60
70	4181.59	4214.56	4247.67	4280.92	70
80	4778.96	4816.64	4854.48	4892.48	80
90	5376.33	5418.72	5461.29	5504.04	90
100	5973.70	6020.80	6068.10	6115.60	100
L.	25.8	25.9	26.0	26.1	L.
10	616.33	621.12	625.93	630.75	10
20	1232.66	1242.24	1251.86	1261.50	20
30	1848.99	1863.36	1877.79	1892.25	30
40	2465.32	2484.48	2503.72	2523.00	40
50	3081.65	3105.60	3129.65	3153.75	50
60	3697.98	3726.72	3755.58	3784.50	60
70	4314.31	4347.84	4381.51	4415.25	70
80	4930.64	4968.96	5007.44	5046.00	80
90	5546.97	5590.08	<b>5633.37</b>	5676.75	90
100	6163.30	6211.20	6259.30	6307.50	100

Supplement to table 4.—Slope 2½ to 1.—Solid contents.

gth.		De	pth.		gth.
Length.	28.6	28.7	28.8	28.9	Length.
10	757.37	762.68	768.00	773.34	10
20	1514.74	1525.36	1536.00	1546.68	20
30	2272.11	2288.04	2304.00	2320.02	30
40	3029.48	3050.72	3072.00	3093.36	40
50	3786.85	3813.40	3840.00	3866.70	50
60	4544.22	4576.08	4608.00	4640.04	60
70	5301.59	5338.76	5376.00	5413.38	70
80	6058.96	6101.44	6144.00	6186.72	80
90	6816.33	6864.12	6912.00	6960.06	90
100	7573.70	7626.80	7680.00	7733.40	100
L.	29.0	29.1	29.2	29.3	<b>L</b> .
10	778.70	784.08	789.48	794.90	10
20	1557.40	1568.16	1578.96	1589.80	20
30	2336.10	2352.24	2368.44	2384.70	30
40	3114.80	3136.32	3157.92	3179.60	40
50	3893.50	3920.40	3947.40	3974.50	50
60	4672.20	4704.48	4736.88	4769.40	60
70	5450.90	5488.56	5526.36	5564.30	70
80	6229.60	6272.64	6315.84	6359.20	80
90	7008.30	7056.72	7105.32	7154.10	90
100	7787.00	7840.80	7894.80	7949.00	100
.L.	29.4	29.5	29.6	29.7	L.
10	800.33	805.79	811.26	816.75	10
20	1600.66	1611.58	1622.52	1633.50	20
<b>3</b> 0	2400,99	2417.37	2433.78	2450.25	30
40	3201.32	3223.16	3245.04	3267.00	40
50	4001.65	4028.95	4056.30	4083.75	50
60	4801.98	4834.74	4867.56	4900.50	60
70	5602.31	<b>564</b> 0.53	5678.82	5717.25	70
80	6402.64	6446.32	6490.08	6534.00	80
90	7202.97	7252.11	7301.34	7350.75	90
100	8003.30	8057.90	8112.60	8167.50	100

## CONTENTS OF SLOPES.

## Supplement to table 4.—Slope $2\frac{1}{2}$ to 1.—Solid contents.

Length.	Depth.			sth.
Len	29.8	29.9	30.0	Length
10	822.26	827.79	833.33	10
20	1644.52	1655.58	1666.66	20
30	2466.78	2483.37	2499.99	30
40	3289.04	3311.16	3333.32	40
50	4111.30	4138.95	4166.65	50
60	4938.56	4966.74	4999.98	60
70	5755.82	5794.53	5833.31	70
80	6578.08	6622.32	6666.64	80
90	7400.34	7450.11	7499.97	90
100	8222.60	8277.90	8333.30	100

Table 5.—Corrections for difference of end depths of Stope for a slope of  $2\frac{1}{2}$  to 1—length 100 feet.

July 10 July 1					
Difference.	Corrections.	Difference.	Corrections.		
		4.0	12.35		
0.1	.01	.1	12.97		
.2	.03	.2	13.61		
.3	.07	.3	14.27		
.4	.12	.4	14.94		
.5	.19	.5	15.62		
.6	.28	.6	16.33		
.7	.38	.7	17.04		
.8	.49	.8	17.78		
.9	.62	.9	18.53		
1.0	.77	5.0	19.29		
.1	.93	.1	<b>20</b> .07		
.2	1.11	.2	20.86		
.3	1.30	.3	21.67		
.4	1.51	.4	22.50		
.5	1.74	.5	23.34		
.6	1.98	.6	24.20		
.7	2.23	.7	<b>25.07</b>		
.8	<b>2.50</b>	.8	<b>25.96</b>		
.9	2.79	.9	26.86		
2.0	3.09	6.0	27.78		
.1	3.40	.1	28.71		
.2	3.73	.2	29.66		
.3	4.08	.3	30.62		
.4	4.44	.4	31.60		
.5	4.82	.5	32.60		
.6	5.22	.6	33.61		
.7	5.62	.7	34.64		
.8	6.05	8.	35.68		
.9	6.49	.9	36.74		
3.0	6.94	7.0	<b>37</b> .81		
.1	7.42	.1	38.90		
.2	7.90	.2	40.00		
.3	8.40	.3	41.12		
.4	8.92	.4	42.25		
.5	9.45	.5	<b>43.4</b> 0		
.6	10.00	.6	44.56		
.7	10.56	.7	45.75		
.8	11.14	.8	46.94		
.9	11.74	.9	48.16		

the 5.—Correction for difference of end depths of Slopes, for a slope of 2½ to 1—length 100 feet.

ference,	Corrections.	Difference.	Corrections.
8.0	49.38	12.0	111.11
.1	50.63	.1	112.97
.2	51.88	.2	114.85
.3	53.16	.3	116.74
.4	54.44	.4	118.64
.5	55.75	.5	120.56
.6	57.07	.6	122.50
.7	58.40	.7	124.45
.8	59.75	-8	126.42
.9	61.12	.9	128.40
9.0	62.50	13.0	130.40
.1	63.90	.1	132.42
.2	65.31	.2	134.44
.3	66.74	.3	136.49
.4	68.18	.4	138.55
.5	69.64	.5	140.63
.6	71.11	.6	142.72
.7	72.60	.7	144.82
.8	74.10	.8	146.94
.9	75.63	.9	149.08
10.0	77.16	14.0	151.23
.1	78.71	.1	153.40
.2	80.28	.2	155.59
.3	81.86	.3	157.79
.4	83.46	.4	160.00
.5	85.07	.5	162.23
.6	86.70	.6	164.48
.7	88.34	.7	166.74
.8	90.00	.8	169.01
.9	91.67	.9	171.30
11.0	93.36	15.0	173.61
.1	95.07	.1	175.93
.2	96.79	.2	178.27
.3	98.53	.3	180.63
.4	100,28	.4	182.99
.5	102.04	.5	185.38
6	103.83	.6	187.78
.7	105.63	.7	190.19
.8	107.44	.8	192.62
.9	109.27	.9	195.07

Table 5.—Corrections for difference of end depths of Slopes, for a slope of 2½ to —length 100 feet.

Difference.	Corrections.	Difference.	Corrections
16.0	197.53	20.0	308.64
.1	200.01	.1	311.74
.2	202.50	.2	314.85
.3	205.01	.3	317.97
.4	207.53	.4	321.11
.5	210.07	.5	324.27
.6	212.62	.6	327.44
.7	215.19	.7	330.63
.8	217.78	.8	333.83
.9	220.38	.9	337.04
17.0	222.99	21.0	340.28
.1	225.63	.1	343.53
.2	228.27	.2	346.79
.3	230.93	.3	350.07
.4	233.61	.4	353.36
.5	236.30	.5	356.67
.6	239.01	.6	360.00
.7	241.74	.7	363.34
.8	244.48	.8	366.70
.9	247.23	.9	370.07
18.0	250.00	22.0	373.46
.1	252.79	.1	376.86
.2	255.59	.2	380.28
.3	258.40	.3	383.71
.4	261.23	.4	387.16
.5	264.08	.5	390.63
.6	266.94	.6	394.10
.7	269.82	7	397.60
.8	272.72	.8	401.11
.9	275.63	.0	404.64
19.0	278.55	23,0	408.18
.1	281.49	.1	411.74
.2	284.44	.2	415.31
.3	287.42	.3	418.90
.4	290.40	.4	422.50
.5	293.40	.5	426.12
.6	296.42	.6	429.75
.7	299.45	.7	433.40
.8	302.50	.8	437.07
9	305.56	9	440.75

ble 5.—Corrections for difference of end depths of Slopes, for a slope of 2½ to 1—length 100 feet.

ference.	Corrections.	Difference.	Corrections.
24.0	444.44	28.0	604.94
.1	448.16	.1	609.27
.2	451.88	.2 .	613.61
.3	455.63	.3	617.97
.4	459.38	.4	622.35
.5	463.16	.5	626.74
.6	466.94	.6	631.14
.7	470.75	.7	635.56
.8	474.57	.8	640.00
.9	478.40	.9	644.45
25,0	482.25	29.0	648.92
.1	486.12	.1	653.40
.2	490.00	.2	657.90
.3	493.90	.3	662.42
.4	497.81	.4	666.94
.5	501.74	.5	671.49
6	505.68	.6	676.05
.7	509.64	.7	680.63
.8	513.61	.8	685.22
.9	517.60	.9	689.82
26.0	521.60	30.0	694.44
.1	525.63	.1	699.08
.2	529.66	.2	703.73
.3	533.71	.3	708.40
.4	537.78	.4	713.09
.5	541.86	.5	717.79
.6	545.96	.6	722.50
.7	550.07	.7	727.23
.8	554.20	.8	731.98
.9	558.34	.9	736.74
27.0	562.50	31.0	741.51
.1	566.67	.1	746.30
.2	570.86	.2	751.11
.3	575.07	.3	755.93
.4	579.29	.4	760.77
.5	583.53	.5	765.63
.6	587.78	.6	770.49
.7	592.04	.7	775.38
.8	586.33 696	3 .8	780.28
O	600.63	.9	785.19

Table 5.—Corrections for difference of end depths of Shan, for a slope of 2½ to 1—length 100 feet.

Difference.	Corrections.	Difference.	Corrections
32.0	790.12	36.0	1000.00
.1	795.07	.1	1005.56
.2	800.03	.2	1011.14
.3	805.01	.3	1016.74
4	810.00	.4	1022.35
.5	815.01	.5	1027.97
.6	820.03	.6	1033.61
.7	825.07	.7	1039.27
.8	830.12	.8	1044.94
.9	835.19	.9	1050.63
33.0	840.28	37.0	1056.33
.1	845.38	.1	1062.04
.2	850.49	.2	1067.78
.3	855.63	.3	1073.53
.4	860.77	.4	1079.29
.5	865.93	.5	1085.07
.6	871.11	.6	1090.86
.7	876.30	.7	1096.67
.8	881.51	.8	1102.50
.9	886.74	.9	1108.34
34.0	891.98	38.0	1114.20
.1	897.23	.1	1120.07
.2	902.50	.2	1125.96
.3	907.79	.3	1131.86
.4	913.09	.4	1137.78
.5	918.40	.5	1143.71
.6	923.73	,6	1149.66
.7	929.08	.7	1155.63
.8	934.44	.8	1161.61
.9	939.82	.9	1167.60
35.0	945.22	39.0	1173.61
.1	950.63	.1	1179.64
.2	956.05	.2	1185.68
.3	961.49	.3	1191.74
.4	966.94	.4	1197.81
.5	972.42	.5	1203.90
.6	977.90	.6	1210.00
.7	983.40	.7	1216.12
.8	988.92	.8	1222.25
.9	994.45	.9	1228.40

Supplement to table 5.—Correction of length average—Slope 21 to 1.

gth.		Dep	ih.		ch.
Length.	0.1	0.2	0.3	0.4	Length.
10			.01	.01	10
20			.02	.02	20
30	•	l	.03	.03	30
40			.04	.04	40
50			05	.05	50
60			.06	.06	60
70		1	.07	.07	70
80		Ì	.08	.08	80
90 1 <b>00</b>	Ì	į.	.09	.09	90
100		1	.10	.10	100
<b>L</b> .	0.5	0.6	0.7	0.8	<b>L</b> .
10	.02	.03	.04	.05	10
20	.04	.06	.08	.10	20
30	.06	.09	.12	.15	80
40	.08	.12	.16	.20	40
<b>50</b> ¸	.10	.15	.20	.25	50
60	.12	.18	.24	.30	60
70	.14	.21	.28	.35	70
80	.1.6	.24	.32	.40	80
90	.18	.27	•36	.45	90
100	.20	.30	.40	.50	100
L.	0.9	1.0	1.1	1.2	<b>L</b> .
10	.06	.08	.09	.11	10
20	.12	.16	.18	.22	20
30	.18	.24	.27	.33	30
40	.24	.32	.36	.44	40
50	.30	.40	.45	.55	50
60	.36	.48	.54	.66	60
70	.42	.56	.63	.77	70
80	.48	.64	.72	.88	80
90	.54	.79	.81	.99	90
100	:60	.80	.90	1.10	100

Supplement to table 5.—Correction of length average—Slope 2½ to 1.

rth.	Depth.					
Length.	1.3	1.4	. 1.5	1.6	Length.	
10	.13	.15	.17	.20	10	
20	.26	.30	.34	.40	20	
30	.39	.45	.51	.60	30	
40	.52	.60	.68	.80	40	
50	.65	.75	.85	1.00	50	
60	.78	.90	1.02	1.20	60	
70	.91	1.05	1.19	1.40	70	
80	1.04	1.20	1.36	1.60	80	
90	1.17	1.35	1.53	1.80	. 90	
100	1.30	1.50	1.70	2.00	100	
<b>L</b> .	1.7	1. 8	1.9	2.0	L.	
10	.22	.25	.28	.31	10	
20	.44	.50	.56	.62	20	
30	.66	.75	.84	.93	30	
40	.88	1.00	1.12	1.24	40	
50	1.10	1.25	1.40	1.55	50	
60	1.32	1.50	1.68	1.86	60	
70	1.54	1.75	1.96	2.17	70	
80	1.76	2.00	2.24	2.48	80.	
90	1.98	2.25	2.52	2.79	90	
100	2.20	2.50	2.80	3:10	100	
. <b>L</b> .	2.1	2.2	2.3	2.4	<b>L</b> .	
10	.34	.37	.41	.44	10	
20	.68	.74	.82	.88	20	
30	1.02	1.11	1.23	1.32	30	
40	1.36	1.48	1.64	1:76	40	
50	1.70	1:85	2.05	2.20	50	
60	2.04	2.22	2.46	2.64	60	
70	2.38	2.59	2.87	3.08	70	
180	2.72	2.96	3.28	8.52	80	
90	8.06	8.33	3.69	<b>3.96</b>	90	
100	3.40	3.70	4.10	4.40	100	

Supplement to table 5.—Correction of length average.—Slope  $2\frac{1}{2}$  to 1.

sth.	Depth.					
Length.	2.5	2.6	2.7	2.8	Length.	
·10	.48	.52	.56	.60	10	
20	96 4	1.04	1.12	1.20	20	
30	1.44	1,56	1.68	1.80	30	
40	1.92	2.08	<b>2.24</b>	2.40	40	
50	<b>2.40</b>	2.60	2.80	3.00	50	
60	2.88	3.12	3.36	3.60	60	
70	3.36	3.64	3.92	4.20	70	
80	3.84	4.16	4.48	4.80	80	
90	<b>4.32</b>	4.68	5.04	5.40	90	
100	4.50	5.20	5.60	6.00	100	
<i>L</i> .	2.9	3.0	3.1	3.2	L.	
10	.65	.69	.74	.79	10	
20	1.30	1.38	1.48	1.58	20	
30	1.95	2.07	2.22	2.37	30	
40	2.60	2.76	2.96	3.16	40	
50	3.25	3.45	3.70	3.95	50	
60	3.90	4.14	4.44	4.74	60	
70	4.55	4.83	5.18	5.53	70	
80	5.20	5.52	5.92	6.32	80	
90	.5.85	6.21	6.66	7.11	90	
100	6.50	6.90	7.40	7.90	100	
L.	3.3	3.4	3.5	3.6	L.	
10	.84	.89	.95	1.00	10	
20	1.68	1.78	1.90	2.00	20	
30	2.52	2.67	2.85	3.00	30	
40	3.36	3.56	3.80	4.00	40	
50	4.20	4.45	4.75	5.00	50	
60	<b>5.04</b>	5.34	5.70	6.00	60	
70	5.88	6.23	6.65	7.00	70	
80	<b>6.72</b>	7.12	7.60	8.00	.80	
90	7.56	8.01	8.55	9.00	90	
100	8.40	8.90	9.50	10.00	180	

Supplement to table 5.—Corrections of length average.—Slope 2½ to 1.

AG W I.						
Length.	Depth.					
Im	3.7	3.8	3.9	4.0	Length.	
10	1.06	1.11	1.17	1.23	10	
20	2.12	2.22	2.34	2.46	20	
30	3.18	3.33	3.51	3.69	30	
40	4.24	4.44	4.68	4.92	40	
50	<b>5.30</b>	5.55	5.85	6.15	50	
60	6.36	6.66	7.02	7.38	60	
70	7.42	7.77	8.19	8.61	70	
80	8.48°	8.88	9.36	9.84	80	
90	9.54	9.99	10.53	11.07	.90	
100	10.60	11.10	11.70	12.30	100	
<b>L</b> .	4.1	4.2	4.3	4.4	L.	
10	1.80	1.36	1.43	1.49	10	
20	2. <b>6</b> 0	2.72	2.86	2.98	20	
30	3.90	4.08	4.29	4.47	30	
40	5.20	5.44	5.72	5.96	40	
50	6.50	6.80	7.15	7.45	50	
60	7.80	8.16	8.58	8.94	60	
70	9.10	9.52	10.01	10.43	70	
80	10.40	10.88	11.44	11.92	80	
90	11.70	12.24	12.87	13.41	90	
100	13.00	13.60	14.80	14-90	100	
<i>L</i> .	4.5	4.6	4.7	4.8	<b>L</b> .	
10	1.56	1.63	1.70	1.78	10	
20	3.12	3.26	3.40	3.56	20	
30	4.68	4.89	5.10	5.34	30	
40	6.24	6.52	6.80	7.12	40	
50	7.80	8.15	8.50	8.90	50	
60	9 <b>.8</b> 6	9.78	10.20	10.68	60	
70	10.92	11.41	11.90	12.46	70	
80	12.48	13.04	- 13.60	14.24	80	
80	14.04	14.67	15. <b>80</b>	16.02	90	
IGO )	15. <b>60</b>	16.30	17.00	17.00	100	

Supplement to table 5.—Correction of length average—Slope : to 1.

gth.	Depth.					
Length.	4.9	5.0	5.1	5.2	Length.	
10	1.85	1.93	2.01	2.09	10	
20	3.70	3.86	4.02	4.18	20	
30	5.55	5.79	6.03	6.27	30	
40	7.40	7.72	8.04	8.36	40	
50	9.25	9.65	10.05	10.45	50	
60	11.10	11.58	12.06	12.54	60	
70	12.95	13.51	14.07	14.63	70	
80	14.80	15.44	16.08	16.72	80	
90	16.65	17.37	18.09	18.81	90	
100	18.50	19.30	20.10	20.90	100	
<i>L</i> .	5.3	5.4	5.5	5.6	<b>L</b> .	
10	2.17	2.25	2.33	2.42	10	
20	4.34	4.50	4.66	4.84	20	
30	6.51	6.75	6.99	7.26	30	
40	8.68	9.00	9.32	9.68	40	
50	10.85	11.25	11.65	12.10	50	
60	13.02	13.50	13.98	14.52	60	
70	15.19	15.75	16.31	16.94	70	
80	17.36	18.00	18.64	19.36	80	
90	<b>19.53</b>	20.25	20.97	21.78	90	
100	21.70	22.50	23.30	24.20	100	
<b>L</b> .	5.7	5.8	5.9	6.0	<b>L</b> .	
10	2.51	2.60	2.69	2.78	10	
20	<b>5.02</b>	5.20	5.38	5.56	20	
30	7.53	7.80	8.07	8.34	30	
40	10.04	10.40	10.76	11.12	40	
50	12.55	13.00	13.45	13.90	50	
60	15.06	15.60	16.14	16.68	60	
70	17.57	18.20	18.83	19.46	70	
80	20.08	20.80	21.52	22.24	80	
90	22.59	23.40	24.21	25.02	90	
100	25.10	26.00	26.90	27.80	100	

Supplement to table 5.—Correction of length average—Slepe  $2\frac{1}{2}$  to 1.

		2 <b>T</b>	10 1.			
gth.	Depth.					
Length.	6.1	6.2	6.3	6.4	Length.	
10	2.87	2.97	3.06	3.16	10	
20	5.74	5.94	6.12	6.32	20	
30	8.61	8.91	9.18	9.48	30	
40	11.48	11.88	12.24	12.64	40	
50	14.35	14.85	15.80	15.80	50	
60	17.22	17.82	18.86	18.96	60	
70	20.09	20.79	21.42	22.12	70	
80	22.96	23.76	24.48	25.28	80	
90	25.88	26.73	27.54	28.44	90	
100	28.70	29.70	30.60	31.60	100	
<b>L</b> .	6.5	6.6	6.7	6.8	<b>L</b> .	
10	3.26	3.36	3.46	3.57	10	
20	6.52	6.72	6.92	7.14	20	
30	9.78	10.08	10.38	10.71	30	
40	13.04	13.44	13.84	14.28	40	
50	16.30	16.80	17.30	17.85	50	
60	19.56	20.16	20.76	21.42	60	
70	22.82	23.52	24.22	24.99	70	
80	26.08	26.88	27.68	28.56	80	
90	29.84	30.24	81.14	32.13	90	
100	<b>32.60</b>	33.60	34.60	35.70	100	
.L.	6.9	7.0	7.1	7.2	L.	
10	3.67	3.78	3.89	4.00	10	
20	7.84	7.56	7.78	8.00	20	
30	11.01	11.34	11.67	12.00,	30	
40	14.68	15.12	15.56	16.00	40	
50	18.35	18.90	19.45	20.00	50	
60	<b>22.02</b>	22.68	23.84	24.00	60	
70	25.69	26.46	27.23	28.00	70	
80	29.36	30.24	31.12	32.00	80	
90	88.03	34,02	<b>85.01</b>	36.00	90	
100	36.70	37.80	38.90	40.00	100	

Supplement to table 5.—Correction of length average.—Slope 2½ to 1.

Length.	Depth.					
La	7.3	7.4	7.5	7.6	Length	
10	4.11	4.23	4.34	4.46	10	
20	8.22	8.46	8.68	8.92	20	
30	12.33	12.69	13.02	13.38	30	
40	16. <del>44</del>	16.92	17.36	17.84	40	
50	20.55	21.15	21.70	22.30	50	
60	24.66	25.38	26.04	26.76	60	
70	28.77	29.61	30.38	31.22	70	
80	<b>32.88</b>	33.84	34.72	35.68	80	
90	<b>36.99</b>	38.07	39.06	40.14	90	
100	41.10	42.30	43.40	44.60	100	
L.	7.7	7.8	7.9	8.0	<b>L</b> .	
10	4.57	4.69	4.82	4.94	10	
20	9.14	9.38	9.64	9.88	20	
30	13.71	14.07	14.46	14.82	30	
40	18.28	18.76	19.28	19.76	40	
50	22.85	23.45	24.10	24.70	50	
60	27.42	28.14	28.92	29.64	60	
70	31. <del>99</del>	32.83	33.74	34.58	70	
80	36.56	37.52	38.56	39.52	80	
90	41.13	42.21	43.38	44.46	90	
100	45.70	46.90	48.20	49.40	100	
<b>L</b> .	8.1	8.2	8.3	8.4	L.	
10	5.06	5.19	5.32	5.44	10	
20	10.12	10.38	10.64	10.88	20	
30	15.18	15.57	15.96	16.32	30	
40	20.24	20.76	21.28	21.76	40	
50	25.30	25.95	26.60	27.20	50	
60	30.36	81.14	81.92	32.64	60	
70	<b>35.42</b>	36.33	37.24	38.08	70	
80	40.48	41.52	42.56	43.52	80	
90	45.54	46.71	47.88	48.96	90	
100	50.60	51.90	53.20	54.40	100	

Supplement to table 5.—Corrections of length average.—Slope  $2\frac{1}{4}$  to 1.

gth.	Depth.					
Length.	8.5	8.6	8.7	8.8	Length.	
10	5.57	5.71	5.84	5.98	10	
20	11.14	11.42	11.68	11.96	20	
30	16.71	17.13	17.52	17.94	30	
40	22.28	22.84	23.36	23.92	40	
50	27.85	28.55	29.20	29.90	50	
60	33.42	34.26	35.04	35.88	60	
70	38.99	39.97	40.88	41.86	70	
.80	<b>44</b> .56	45.68	46.72	47.84	80	
90	50.13	51.39	52.56	53.82	90	
100	55.70	57.10	58.40	59.80	100	
L.	8.9	9.0	9.1	9.2	L.	
10	6.11	6.25	6.39	6.53	10	
20	12.22	12.50	12.78	13.06	20	
30	18.33	18.75	19.17	19.59	30	
40	24.44	25.00	25.56	26.12	40	
50	. <b>30.55</b>	31.25	31.95	32.65	50	
60	<b>36.66</b>	37.50	38.34	39.18	60	
70	42.77	43.75	44.73	45.71	70	
80	48.88	50.00	51.12	52.24	80	
90	<b>54.99</b>	<b>56.25</b>	57.51	58.77	90	
100	61.10	62.50	63.90	65.30	100	
L.	9.3	9.4	9.5	9.6	<b>L</b> .	
10	6.67	6.82	6.96	7.11	10	
20	13.34	18.64	13.92	14.22	20	
30	20.01	20.46	20.88	21.33	30	
40	<b>26</b> .68	27.28	27.84	28.44	40	
<b>50</b>	33.35	34.10	34.80	35.55	50	
60	40.02	40.92	41.76	42.66	60	
70	46.69	47.74	48.72	49.77	70	
80	58.36	54.56	55.68	56.88	80	
90	60.03	61.38	62.64	63.99	90	
100	66.70	68.20	69.60	71.10	100	

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Supplement to table 5.—Corrections of length average.—Slope 2½ to 1.

1	<del></del>	~,	.,		ī.		
gth		Depth.					
Length.	9.7	9.8	9.9	10.0	Length.		
10	7.26	7.41	7.56	7.72	10		
20	14.52	14.82	15.12	15.44	20		
30	21.78	22.23	22.68	23.16	30		
40	29.04	29.64	30.24	30.88	40		
50	36.30	37.05	37.80	38.60	50		
60	43.56	44.46	45.36	46.32	60		
70	50.82	51.87	52.92	54.04	70		
80	58.08	59.28	60.48	61.76	80		
90	65.34,	66.69	68.04	69.48	90		
100	72.60	74.10	75.60	77.20	100		
L.	10.1	10.2	10.3	10.4	<b>L</b> .		
10	7.87	8.03	8.19	8.35	10		
20	15.74	16.06	16.38	16.70	20		
30	23.61	24.09	24.57	25.05	30		
40	31.48	32.12	32.76	33.40	40		
50	<b>3</b> 9.35	40.15	40.95	41.75	50		
60	47.22	48.18	49.14	50.10	60		
70	55.09	56.21	57.33	58.45	70		
80	<b>6</b> 2. <del>9</del> 6	64.24	65.52	66.80	80		
90	70.83	72.27	78.71	75.15	90		
100	78.70	80.30	81.90	83.50	100		
L.	10.5	10.6	10.7	10.8	<b>L</b> .		
10	8.51	8.67	8.83	9.00	10		
. 20	- 17.02	17.34	17.66	18.00	20		
30	25.53	26.01	26.49	27.00	30		
40	34.04	34.68	35.32	36.00	40		
50	42.55	43.35	44.15	45.00	50		
60	51.06	52.02	52.98	54.00	60		
70	59.57	60.69	61.81	63.00	70		
80	68.08	69.86	70.64	72.00	80		
90	76.59	78.03	79.47	81.00	90		
400	85.10	86.70	88.80	90.00	100		

Supplement to table 5.—Corrections of length average.—Slope 2½ to 1.

th.		De	pth.		gth.
Length.	10.9	11.0	11.1	11.2	Length.
10	9.17	9.34	9.51	9.68	10
20	18.34	18.68	19.02	19.36	20
30	27.51	28.02	28.53	29.04	30
40	36.68	37.36	38.04 ·	38.72	40
50	45.85	46.70	47.55	48.40	50
60	55.02	56.04	57.06	58.08	60
70	64.19	65.38	66.57	67.76	70
80	73.36	74.72	76.08	77.44	80
90	82.53	84.06	85.59	87.12	90
100	91.70	98.40	95.10	96.80	100
L.	11.3	11.4	11.5	11.6	<b>L</b> .
10	9.85	10.03	10.20	10.38	10
20	19.70	20.06	20.40	20.76	20
30	29.55	30.09	30.60	81.14	30
40	39.40	40.12	40.80	41.52	40
50	49.25	50.15	51.00	51.90	50
60	59.10	60.18	61.20	62.28	60
70	68.95	70.21	71.40	72.66	70
80	78.80	80.24	81.60	83.04	80
90	88.65	90.27	91.80	93.42	99
100	98.50	100.30	102.00	103.90	100
L.	11.7	11.8	11.9	12.0	L.
10	10.56	10.74	10.93	11.11	10
20	21.12	21.48	21.86	22.22	20
30	<b>31.6</b> 8	32.22	32.79	33.33	30
40	42.24	42.96	43.72	44.44	40
50	<b>52.8</b> 0	53.70	<b>54.6</b> 5	<b>55.5</b> 5	50
60	<b>63.3</b> 6	64.44	65.58	66.66	60
70	73.92	75.18	76.51	77.77	70
80	84.48	85.92	87.44	88.88	80
90	95.04	96.66	98.37	99.99	90
200	105.60	107.40	109.30	111.40	100

Supplement to table 5.—Correction of length average.—Slope  $2\frac{1}{4}$  to 1.

gth.	Depik.					
Length.	12.1	12.2	12.3	12.4	Length.	
10	11.30	11.48	11.67	11.86	10	
20	22.60	22.96	23.34	23.72	20	
30	33.90	34.44	35.01	35.58	30	
40	45.20	45.92	46.68	47.44	40	
50	56.50	57.40	58.35	59.30	50	
60	67.80	68.88	70.02	71.16	60	
70	79.10	80.36	81.69	83.02	70	
80	90.40	91.84	93.36	94.88	80	
90	101.70	103.32	105.03	106.74	90	
100	113.00	114.80	116.70	118.60	100	
L.	12.5	12.6	12.7	12.8	L.	
10	12.06*	12.25	12.45	12.64	10	
20	24.12	24.50	24.90	25.28	20	
30	36.18	36.75	37.35	37.92	30	
40	48.24	49.00	49.80	50.56	40	
50	60.30	61.25	62.25	63.20	50	
60	72.36	73.50	74.70	75.84	60	
70	84.42	85.75	87.15	88.48	70	
80	96.48	98.00	99.60	101.12	80	
90	108.54	110.25	112.05	113.76	90	
100	120.60	122.50	124.50	126.40	100	
L.	12.9	13.0	13.1	13.2	<b>L</b> .	
10	12.84	13.04	13.24	13.44	10	
20	25.68	26.08	26.48	26.88	20	
30	38.52	39.12	39.72	40.32	30	
40	51.36	52.16	52.96	58.76	40	
50	64.20	65.20	66.20	67.20	50	
60	77.04	78.24	79.44	80.64	60	
70	89.88	91.28	92.68	94.08	70	
80	102.72	104.32	105.92	107.52	80	
90	115.56	117.36	119.16	120.96	90	
100	128.49	130.40	132.40	134.40	100	

Supplement to table 5.—Correction of length average.—Slope 21 to 1.

Length.	Depth.					
Len	13.3	13.4	18.5	13.6	Length.	
10	13.65	13.85	14.06	14.27	10	
20	27.30	27.70	28.12	28.54	20	
<b>3</b> 0	40.95	41.55	42.18	42.81	30	
40	54.60	55.40	56.24	57.08	40	
50	68.25	69.25	70.30	71.35	50	
60	81.90	83.10	84.36	85.62	60	
70	95.55	96.95	98.42	99.89	70	
80	109.20	110.80	112.48	114.16	80	
90	122.85	124.65	126.54	128.43	90	
100	136.50	138.50	140.60	142.70	100	
L.	13.7	13.8	13.9	14.0	Į.	
10	14.48	14.69	14.91	16.12	10	
20	28.96	29.38	29.82	30.24	20	
30	43.44	44.07	44.73	45.36	30	
40	57.92	58.76	59.64	60.48	40	
50	72.40	73.45	74.55	75.60	50	
60	86.88	88.14	89.46	90.72	60	
70	101.36	102.83	<b>≠</b> 104.37	105.84	70	
80	115.84	117.52	119.28	120.96	80	
90	130.32	132.21	134.19	136.08	90	
100	144.80	146.90	149.10	151.20	100	
L.	14.1	14.2	14.3	14.4	L.	
10	15.34	15.56	15.78	16.00	10	
20	30.68	31.12	31.56	32.00	20	
30	46.02	46.68	47.34	48.00	30	
<b>4</b> 0	61.36	62.24	63.12	64.00	40	
<b>5</b> 0	76.70	77.80	78.90	80.00	50	
<b>6</b> 0	92.04	93.36	94.68	96.00	60	
70	107.38	108.92	110.46	112.00	70	
80	132.72	124.48	126.24	128.00	80	
90	138,06	140.04	142.02	144.00	90	
100	153.40	155.60	157.80	160.00	100	

Supplement to Table V.—Correction of Length Average.—Slope 24 to 1.

th.	Depth.				
Length.	14.5	14.6	14.7	14.8	Length.
10	16.22	16.45	16.67	16 90	10
20	32.44	32.90	33,34	33.80	20
30	48.66	49.35	50.01	50.70	30
40	64.88	65.80	66.68	67.60	40
50	81.10	82.25	83 35	84.50	50
60	97.32	98.70	100.02	101.40	60
70	113.54	115.15	116.69	118.30	70
80	129.76	131.60	133.36	135.20	80
90	145.98	148.05	150.03	152.10	90
100	162.20	164.50	166.70	169.00	100
L.	14.9	15.0	15.1	15.2	L.
10	17.13	17.36	17.59	17.83	10
20	34.26	34.72	35.18	35.66	20
30	51.39	52.08	52.77	53.49	30
40	68.52	69.44	70.36	71.32	40
50	85.65	86.80	87.95	89.15	50
60	102.78	104.16	105.54	106.98	60
70	119.91	121.52	123.13	124.81	70
80	137.04	138.88	140.72	142.64	80
90	154.17	156.24	158.31	160.47	90
100	171.30	173.60	175.90	178.30	100
<i>L</i> .	15.3	15.4	15.5	15.6	L.
10	18.06	18.30	18.54	18.78	10
20	36.12	36.60	37.08	37.56	20
30	54.18	54.90	55.62	56.34	30
40	72.24	73.20	74.16	75.12	40
50	90.30	91.50	92.70	93.90	50
60	108.36	109.80	111.24	112.68	60
70	126.42	128.10	129.78	131.46	70
80	144.48	146.40	148.32	150 24	80
90	162.54	164.70	166.86	169.02	90
100	180.60	183.00	185.40	187.80	100
	15				

Table VI.—Embankment.—Roadway 14 feet wide.—Side Slopes 11 to 1.

Depths.	Contents.	Depths.	Contents.	Depths.	Contents.
		20.0	3259	40.0	10963
0.5	27	.5	3398	.5	11212
1.0	57	21.0	3539	41.0	11465
.5	90	.5	3683	.5	11720
20	126	22.0	3830	42.0	11978
.5	164	.5	3979	.5	12238
3.0	206	23.0	4131	43.0	12502
.5	250	.5	4287	5	12768
4.0	296	24.0	4444	44.0	13037
.5	346	.5	4605	.5	13309
5.0	398	25.0	4768	45.0	13 <b>583</b>
.5	453	.5	4935	.5	13861
6.0	511	26.0	5104	46.0	14141
.5	572	.5	5275	.5	14424
7.0	63 <b>5</b>	27.0	5450	47.0	14709
.5	701	.5	5627	.5	14998
8.0	770	28.0	5807	48.0	15289
.5	842	.5	5990	.5	15583
9.0	917	29.0	6176	49.0	15880
.5	994	.5	6364	.5	16179
10.0	1074	30.0	6555	50.0	16481
•5	1157	.5	6749	.5	16787
11.0	1243	31.0	6946	51.0	17094
.5	1331	.5	7146	.5	17405
12.0	1422	32.0	7348	52.0	17719
.5	1516	.5	7553	.5	18035
13.0	1613	33.0	7761	53.0	18354
.5	1713	.5	7972	.5	18675
14.0	1815	34.0	8185	54.0	19000
•5	1920	.5	8401	.5	19327
15.0	2028	35.0	8620	55.0	19657
.5	2138	.5	8842	.5	19990
16.0	2252	36.0	9067	56.0	20326
.5	2368	.5	9294	.5	20664
17.0	2487	37.0	9524	57.0	21006
.5	2609	.5	9757	.5	21350
18.0	2733	38.0	9993	58.0	21696
.5	2861	.5	10231	.5	22046
19.0	2991	39.0	10472	59.0	22398
.5	3124	.5	10716	.5	22753

Tuble VII.—Embankment.—Roadway 15 feet wide.—Side Slopes 1½ to

Depths.	Contents.	Depths.	Contents.	Depths.	Contents.
		20.0	3333	40.0	11111
0.5	29	.5	3474	.5	11362
1.0	61	21.0	3617	41.0	11617
.5	96	.5	3762	.5	11874
2.0	133	22.0	3911	42.0	12133
.5	174	.5	4063	.5	12396
3.0	217	23.0	4217	43.0	12661
.5	262	.5	4374	.5	12929
4.0	311	24.0	4533	44.0	13200
.5	363	.5	4696	.5	13474
5.0	417	25.0	4861	45.0	13750
.5	474	.5	5029	.5	14029
6.0	533	26.0	5200	46.0	14311
.5	596	.5	5374	.5	14596
7.0	661	27.0	5550	47.0	14883
.5	729	.5	5729	.5	15174
8.0	800	28.0	5911	48.0	15467
.5	874	.5	6096	.5	15763
9.0	950	29.0	6283	49.0	16061
.5	1029	.5	6474	.5	16363
10.0	1111	30.0	6667	50.0	16667
.5	1196	.5	6862	.5	16974
11.0	1283	31.0	7061	51.0	17283
.5	1374	.5	7263	.5	17596
12.0	1467	32.0	7467	52.0	17911
.5	1562	.5	7674	.5	18229
13.0	1661	33,0	7883	53.0	18550
.5	1763	.5	8096	.5	18874
14.0	1867	34.0	8311	54.0	19200
.5	1974	.5	8529	.5	19529
15.0	2083	35.0	8750	55.0	19861
.5	2196	.5	8974	.5	20196
16.0	2311	36.0	9200	56.0	20533
.5	2429	.5	9429	.5	20874
17.0	2550	37.0	9661	57.0	21217
.5	2674	.5	9896	.5	21562
18.0	2800	38.0	10133	58.0	21911
.5	2929	.5	10374.	.5	22263
19.0	3061	39.0	10617	59.0	22617
.5	3196	.5	10862	.5	22974

Table VIII.—Excavation.—Roadway 20 feet wide.—Side Slopes 11 to 1.

Depths.	Contents.	Depths.	Contents.	Depths.	Contents.
		20.0	3333	40.0	10370
0.5	38	.5	3464	.5	10594
1.0	79	21.0	. 3597	41.0	10819
.5	122	.5	3733	.5	11047
2.0	167	22.0	3870	42.0	11278
.5	214	.5	4010	.5	11510
3.0	264	23.0	4153	43.0	11745
.5	316	.5	4297	.5	11983
4.0	370	24.0	4444	44.0	12222
.5	427	.5	4594	.5	12464
5.0	486	25.0	4745	45.0	12708
.5	547	.5	4899	.5	12955
6.0	611	26.0	5056	46.0	13204
.5	677	.5	5214	.5	13455
7.0	745	27.0	5 <b>37</b> 5	47.0	13706
.5.	816	.5	5538	.5	13964
8.0	889	28.0	5704	48.0	14222
.5	964	.5	5872	.5	14483
9.0	1042	29.0	6042	49.0	14745
.5	1122	.5	6214	.5	15010
10.0	1204	30.0	6389	50.0	15278
.5	1288	.5	6566	.5	15547
11.0	1375	31.0	6745	51.0	15819
.5	1464	.5	6927	.5	16094
12.0	1556	32.0	7111	52.0	16370
-5	1649	.5	7297	.5	16649
13.0	1745	33.0	7486	53.0	16931
.5	1844	.5	7677	.5	17214
14.0	1944	34.0	7870	54.0	17500
.5	2047	.5	8066	.5	17788
15.0	2153	35.0	8264	55.0	18079
.5	2260	.5	8464	.5	18372
16.0	2370	36.0	8667	56.0	18667
.5	2483	.5	8872	.5	18964
17.0	2597	37.0	9079	57.0	19264
.5	2714	.5	9288	.5	19566
18.0	2833	38.0	9500	58.0	19870
.5	2955	.5	9714	.5	20177
19.0	3079	39.0	9931	59.0	20486
.5	3205	.5	10149	.5	20797

Table IX.—Excavation.—Roadway 22 feet wide.—Side Slopes ‡ to

Depths.	Contents.	Depths.	Contents.	Depths.	Contents
		20.0	3481	40.0	10666
0.5	42	.5	3616	.5	10894
1.0	86	21.0	3753	41.0	11123
.5	133	.5	3892	.5	11355
2.0	181	22.0	4033	42.0	11589
.5	233	.5	4177	.5	11825
3.0	286	23.0	4323	43.0	12064
.5	342	.5	4472	.5	12305
4.0	400	24.0	4622	44.0	12548
.5	460	.5	4775	.5	12794
5.0	523	25.0	4931	45.0	13042
.5	588	.5	5088	.5	13292
6.0	656	26.0	5248	46.0	13544
.5	725	.5	5410	.5	13799
7.0	797	27.0	5575	47.0	14056
.5	872	.5	5742	.5	14316
8.0	948	28.0	5911	48.0	14578
.5	1027	.5	6083	.5	14842
9.0	1108	29.0	6256	49.0	15108
.5	1192	.5	6433	.5	15377
10.0	1278	30.0	6611	50.0	15648
.5	1366	.5	6792	.5	15922
11.0	1456	31.0	6975	51.0	16197
.5	1549	.5	7160	.5	16475
12.0	1644	32.0	7348	52.0	16756
.5	1742	.5	7538	.5	17038
13.0	1842	33.0	7731	53.0	17323
.5	1944	.5	7925	.5	17610
14.0	2048	34.0	8122	54:0	17900
.5	2155	.5	8322	.5	18192
15.0	2264	35.0	8523	55.0	18486
.5	2375	.5	8727	.5	18783
16.0	2489	36.0	8933	56.0	19081
.5	2605	.5	9142	.5	19383
17.0	2723	37.0	9353	57.0	19686
.5	2844	.5	9566	.5	19992
18.0	2967	38.0	9781	58.0	20300
.5	3092	.5	9999	.5	20610
19.0	3219	39.0	10219	59.0	20923
.5	3349	.5	10442	.5	21238

